



# Precipitation Models

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# Outline

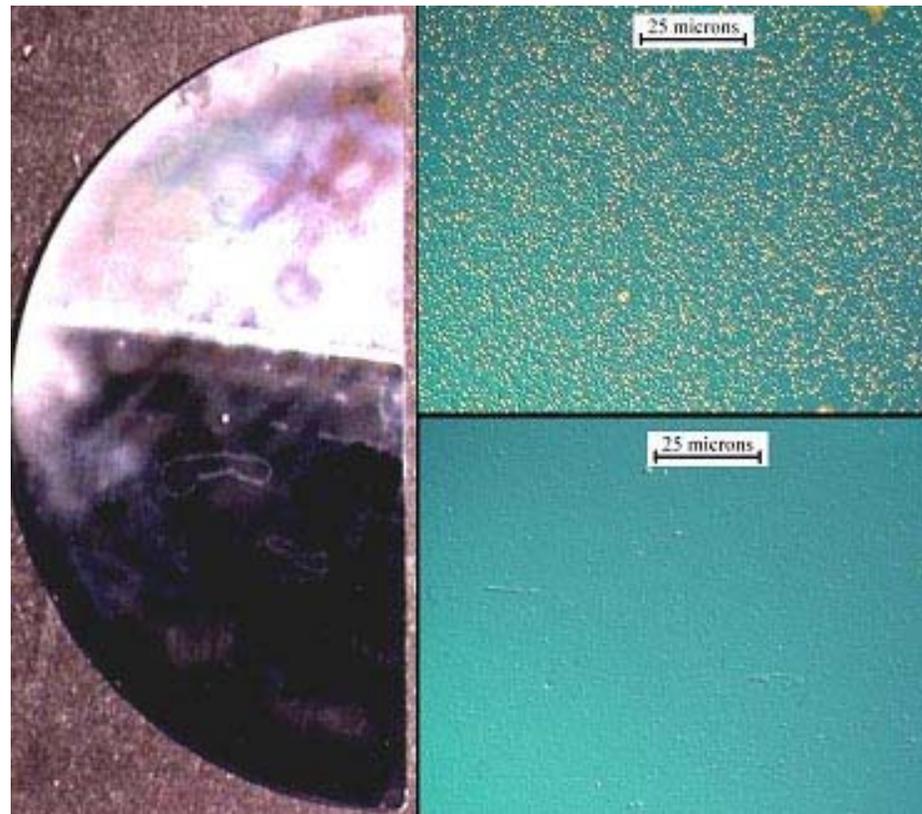
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- ◆ **Motivation**
  - Precipitation in Silicon
  - Why Do We Care?
  - TCAD: Technology Computer-Aided Design
- ◆ The Problem
- ◆ Modeling of Precipitation
- ◆ Reduced Kinetic Precipitation Model
- ◆ RKPM Example: Dislocations
- ◆ Oxygen Precipitation



# Precipitation in Silicon

At sufficiently high concentrations, impurity atoms want to “stick” together to lower their energy, forming their own phase.

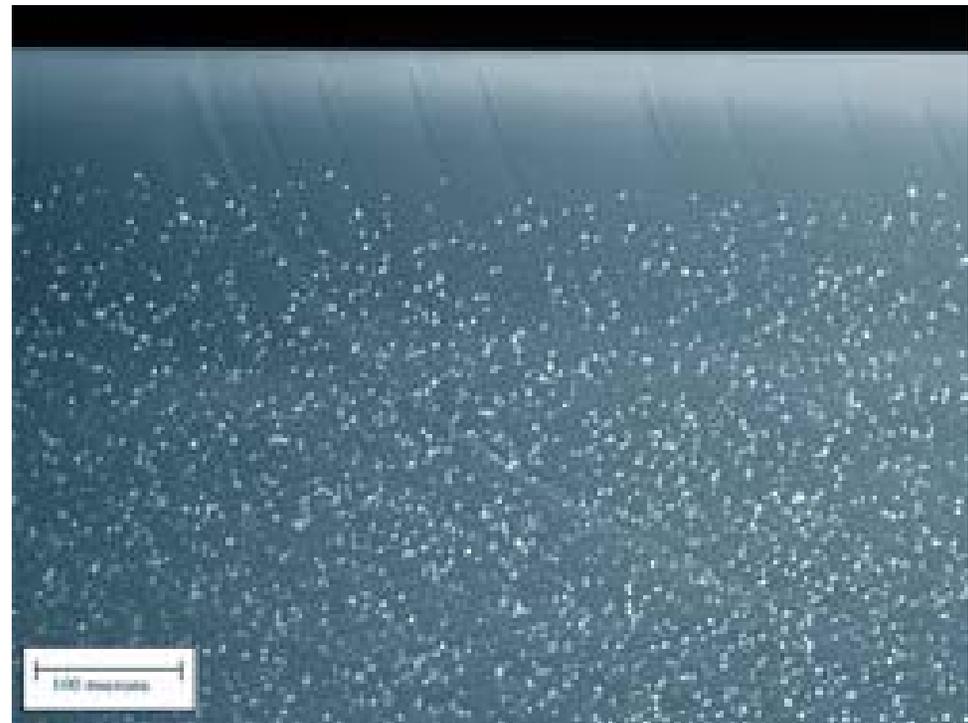
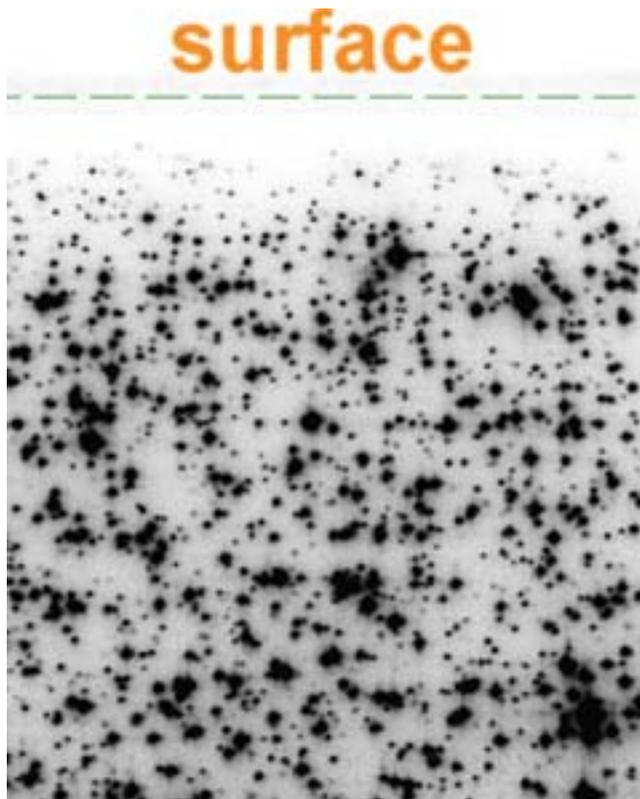


*Copper precipitates on the surface of a silicon wafer.*



# Precipitation in Silicon

Oxygen is present in CZ-grown silicon, which is widely used in the VLSI and PV industries.

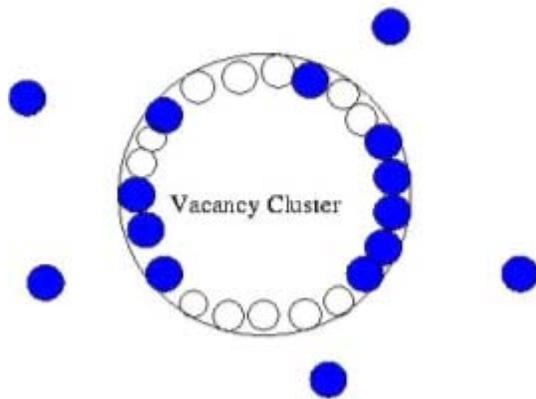


*Cross-sectional images of oxygen precipitates in wafers.*

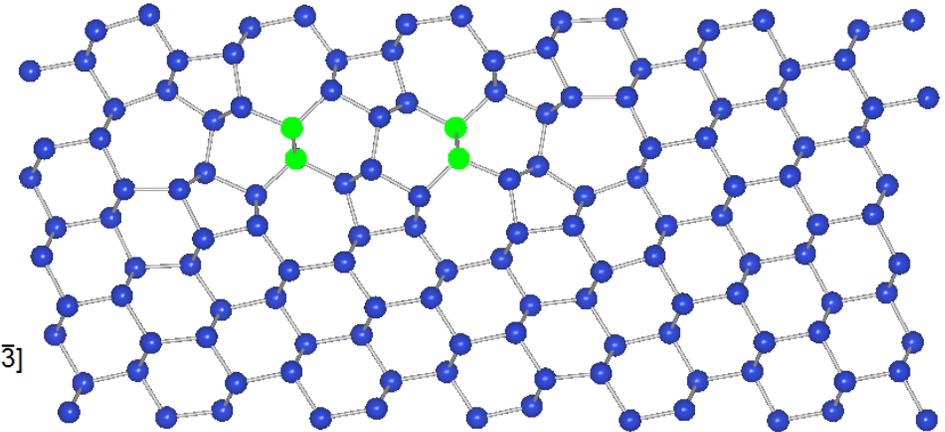


# Precipitation in Silicon

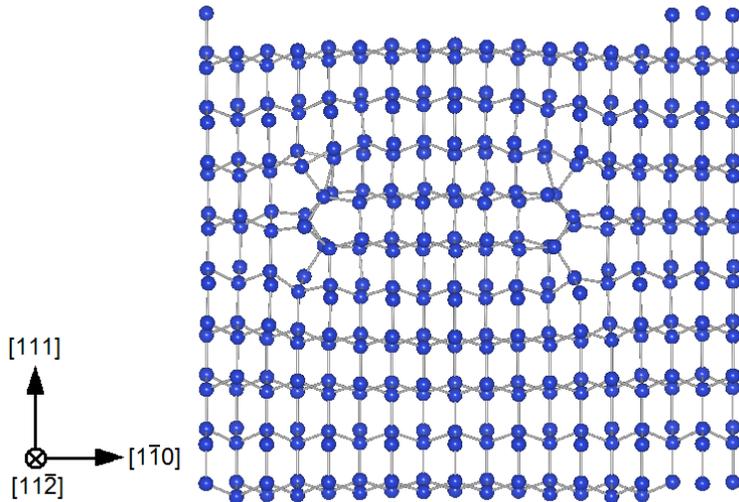
Extended defects are precipitates, too.



[311]  
[011] → [233]



Above:  $\{311\}$  defect chains (green).  
Left: Faulted edge dislocation.





# Why Do We Care?

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## ◆ Metals

- Shallow donors (esp. Cu)
- Recombination active
- Fast diffusing, may segregate to active areas of device

## ◆ Oxygen

- Improves stiffness
  - ◆ Wafers less susceptible to slip and warp during high-T processing
- Oxygen interstitials form thermal (shallow) donor defects
- BO<sub>2</sub> clusters
  - ◆ Highly recombination-active, big concern in PVs
- Dislocation nucleation

## ◆ Extended defects

- Act as sinks for silicon interstitials, impurities, dopants



# The Problem

- ◆ Nucleation/growth models require a solution for each possible precipitate size. Dozens or hundreds of equations!

$$\frac{df_1}{dt} = -2I_1 - \sum_{i=2}^{\infty} I_i$$

$$\frac{df_n}{dt} = I_{n-1} - I_n$$

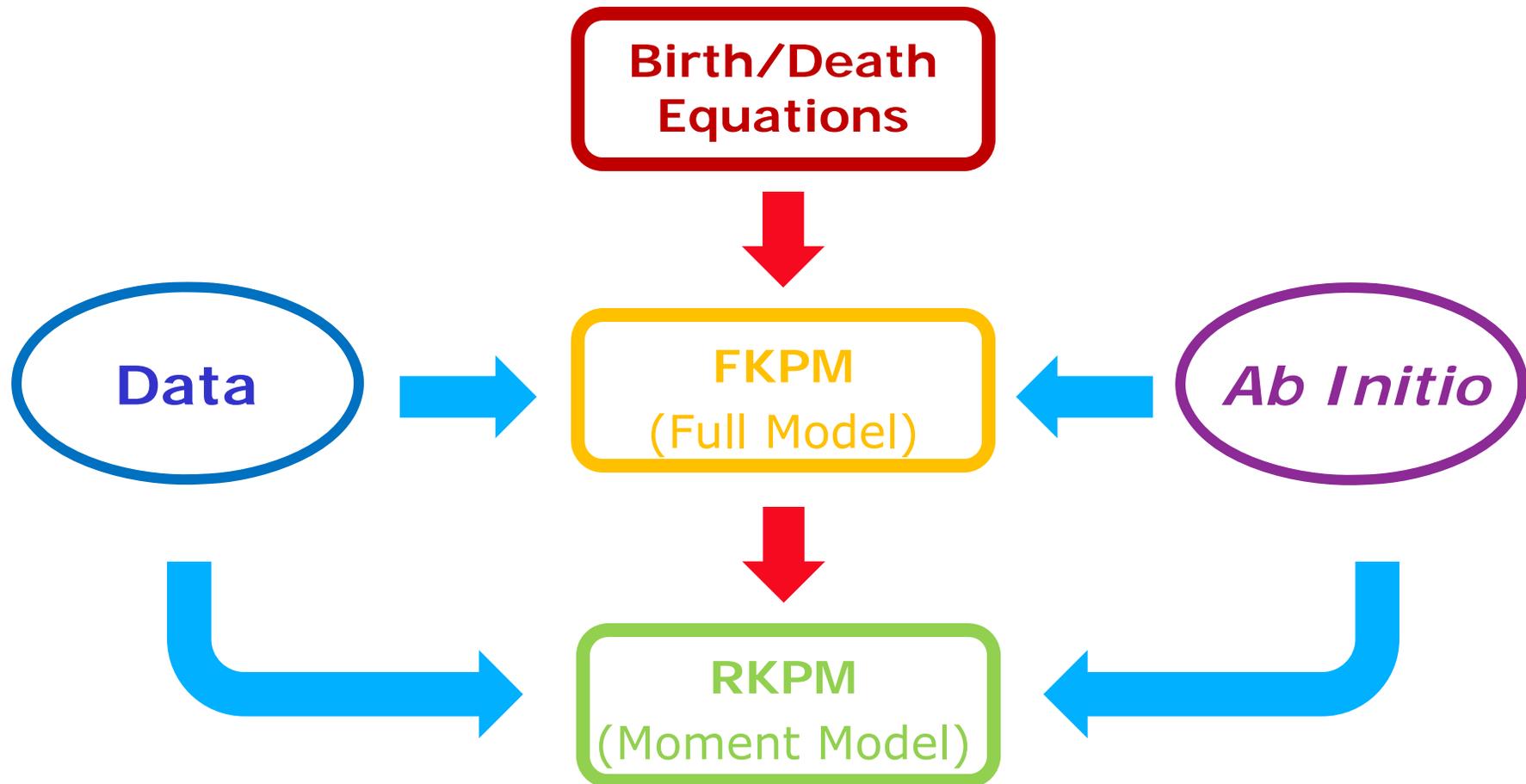
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- ◆ Device geometries (esp. 2D and 3D) can have hundreds of sample points. **Computationally intractable.**
- ◆ **No stress dependence.**



# The Solution

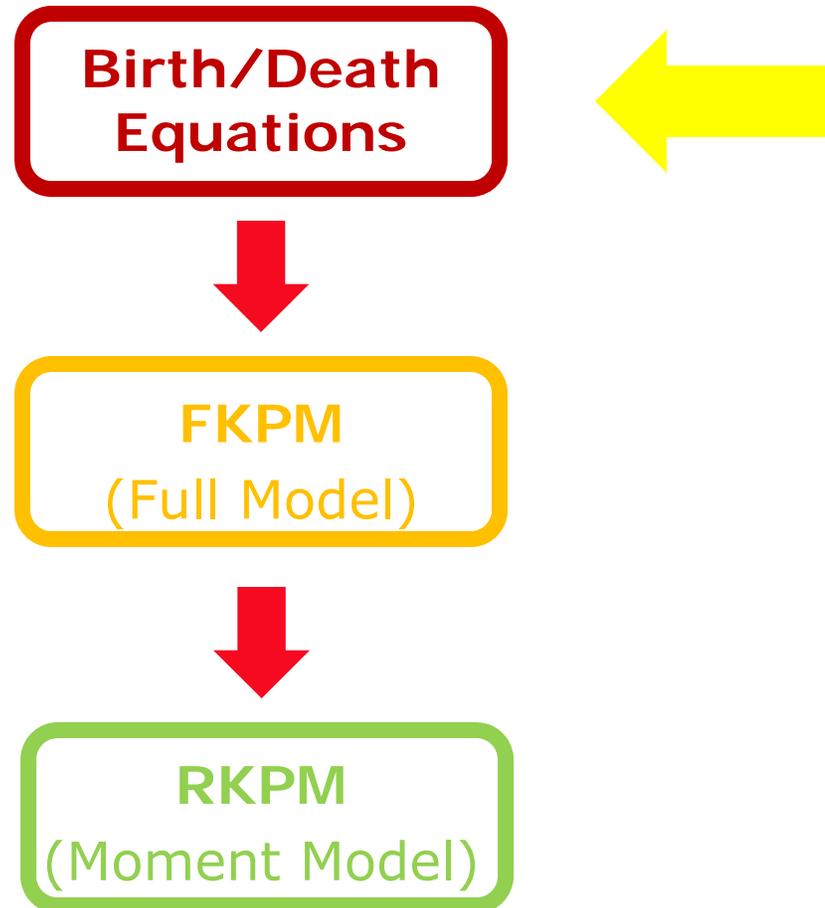
Development of a moment-based (RKPM) model.





# Modeling Flowchart

Development of a moment-based (RKPM) model.





# Precipitate Energetics

## ◆ Precipitate free energy

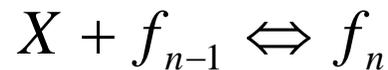
- $C$ : Solute concentration (e.g., interstitial oxygen atoms)
- $C_{ss}$ : Solid solubility (want to precipitate when solute concentration exceeds this)
- $G_{exc}(n)$ : Excess (surface) energy.

$$G_n = -n \cdot kT \ln \frac{C}{C_{ss}} + G_{exc}(n)$$



# Growth Kinetics

- ◆ Nucleation and growth reactions



- ◆ Solute concentration at equilibrium with precipitate of size  $n$

$$C_n^* = C_{SS} \exp\left\{\frac{-(G_n - G_{n-1})}{kT}\right\}$$



# Full Kinetic Precipitation Model

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Birth/death equation for each possible precipitate size:

$$\frac{\partial f_2}{\partial t} = g_1 \cdot C - d_2 f_2 - (g_2 f_2 - d_3 f_3)$$

$$\frac{\partial f_3}{\partial t} = g_2 f_2 - d_3 f_3 - (g_3 f_3 - d_4 f_4)$$

...

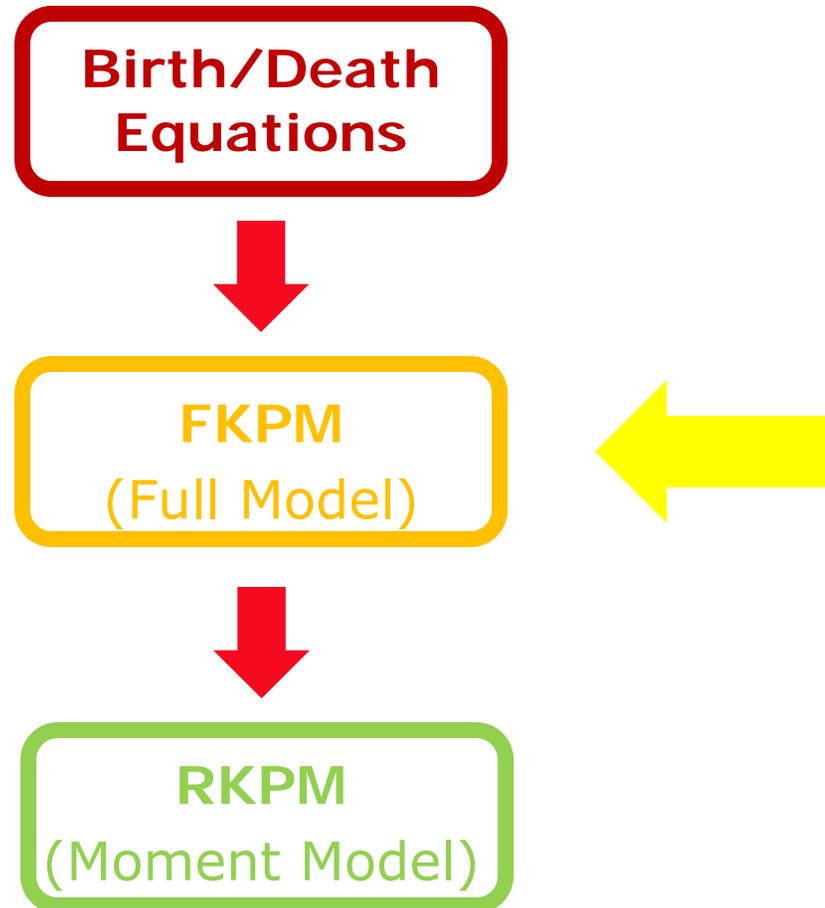
**Problem: Too many equations!**

**Solution: Discretization.**



# Modeling Flowchart

Development of a moment-based (RKPM) model.

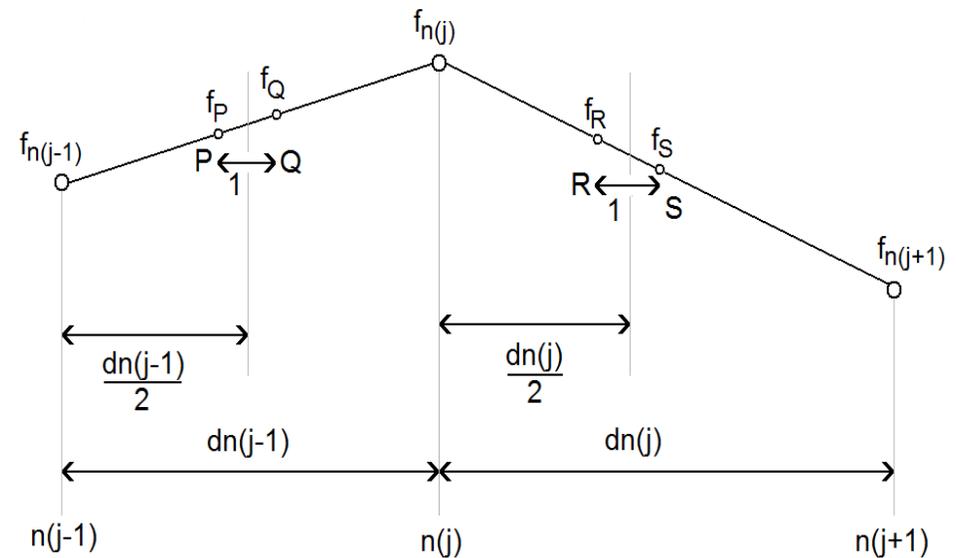
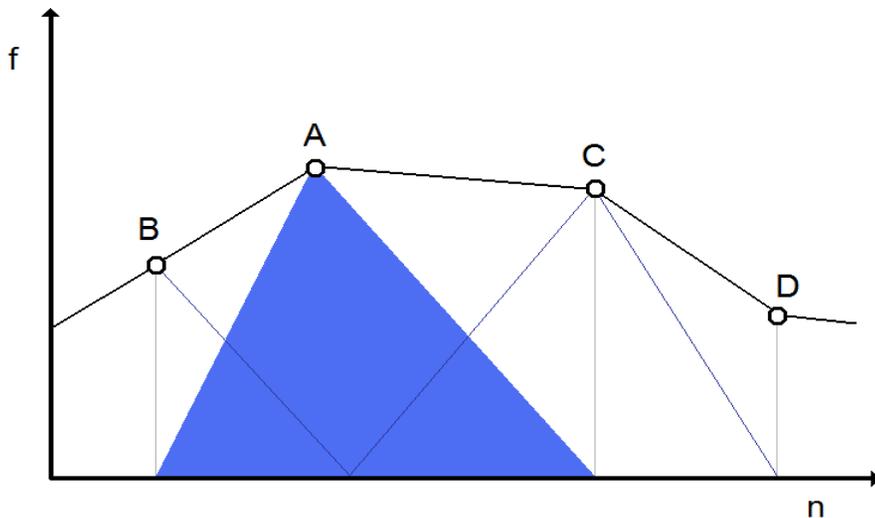




# Discretization

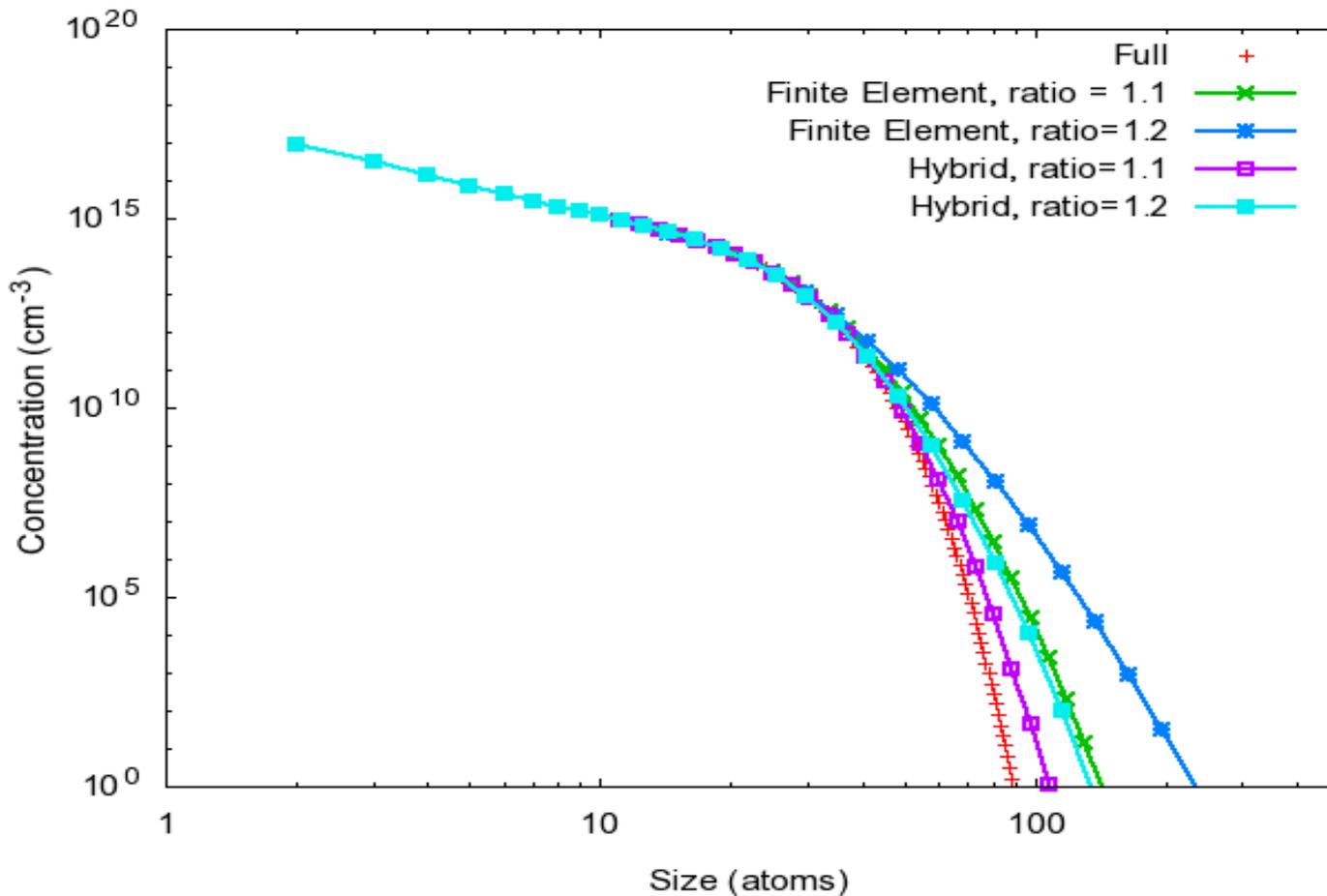
Sample in size space. Compute samples w/ interpolation:

- Linear
- Exponential
- Finite element (linear)
- Hybrid (FEM, exponential)





# Discretization



*Comparison of different discretization methods.*



# Outline

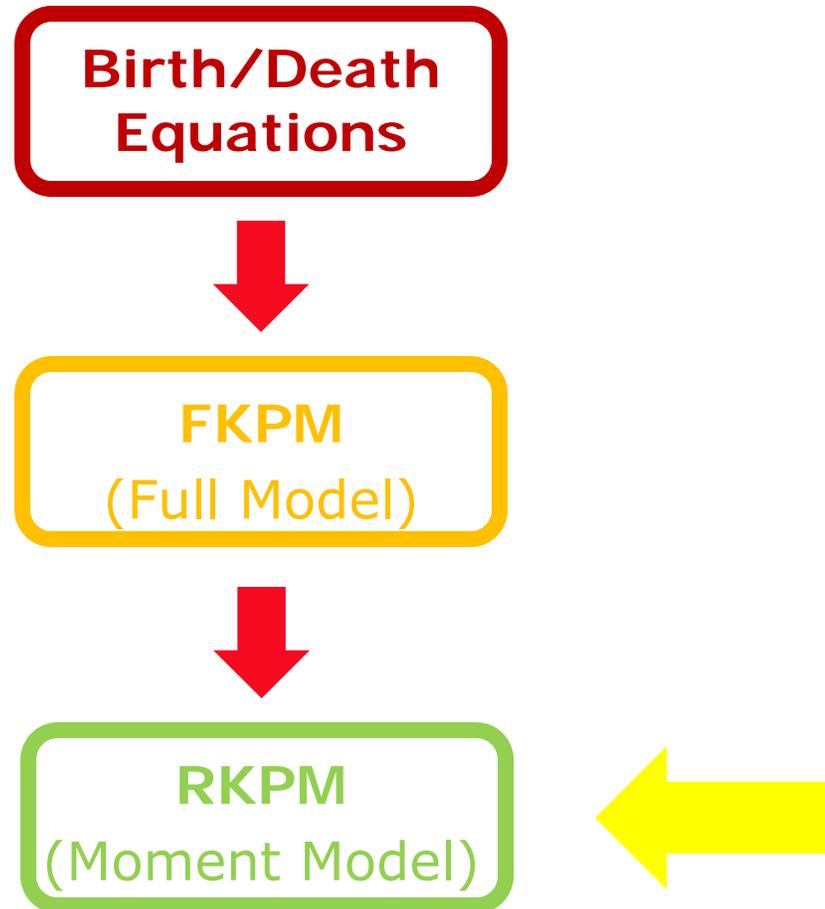
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- ◆ Motivation
- ◆ The Problem
- ◆ Modeling of Precipitation
- ◆ **Reduced Kinetic Precipitation Model**
  - **A More Efficient Approach**
  - **Closure Assumptions**
- ◆ RKPM Example: Dislocations
- ◆ Oxygen Precipitation
- ◆ Proposed Research



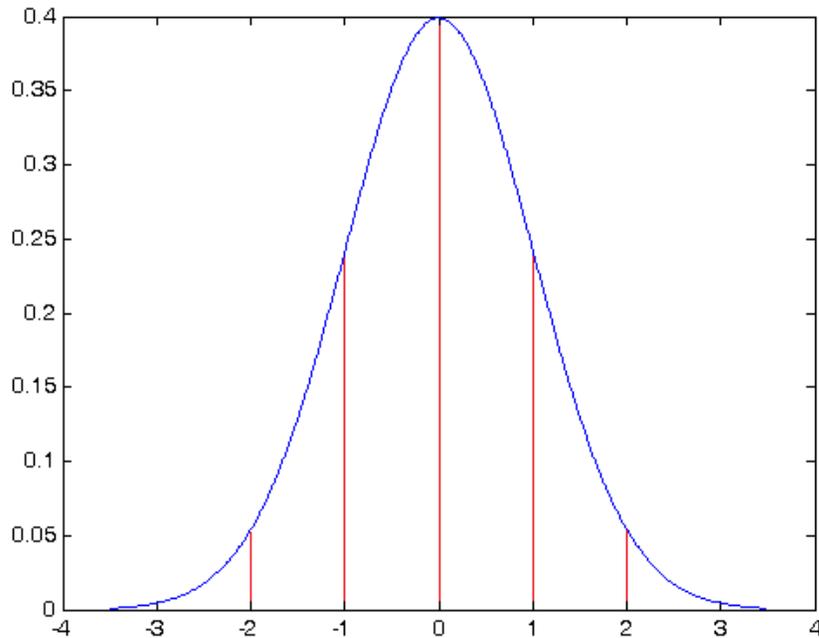
# Modeling Flowchart

Development of a moment-based (RKPM) model.

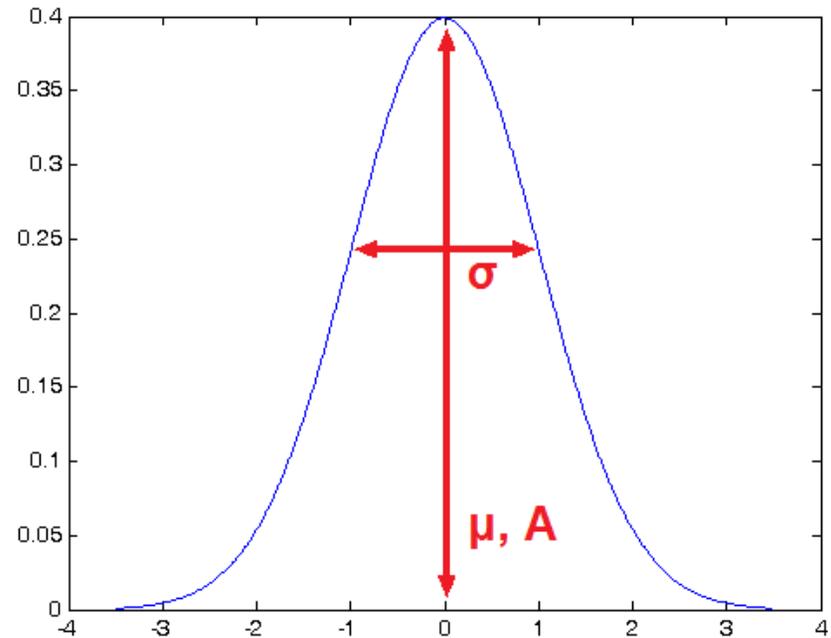




# A More Efficient Approach



We *could* track every possible defect size independently (conceptually easy)...



... but why not be more clever about it and track only the bare minimum of information needed to describe a distribution?



# Growth Rate

## ◆ Growth rate [3]

$$I_{n-1} = D_I \lambda_{n-1} (C_I f_{n-1} - C_n^* f_n)$$

- $D_I$ : Diffusivity of interstitials
- $C_I$ : Interstitial concentration
- $\lambda_n$ : A kinetic growth factor
- $C_n^*$ : Local equilibrium constant associated with size- $n$  defects for interstitials

$$C_n^* = C_{SS} \exp \left\{ - \frac{(\Delta G_n^{exc} - \Delta G_{n-1}^{exc})}{k_B T} \right\}$$

## ◆ Change in free energy upon defect formation

$$\Delta G_n = -n \cdot k_B T \ln \frac{C_I}{C_{SS}} + \Delta G_n^{exc}$$

- $C_{SS}$ : Solid solubility
- $\Delta G_n^{exc}$ : Excess formation energy (perimeter)



# RKPM

## ◆ Continuity equations rewritten in terms of moments

$$\frac{dm_i}{dt} = k^i I_{k-1} + \sum_{n=k}^{\infty} [(n+1)^i - n^i] I_n = k^i I_{k-1} + D_I m_0 (C_I \gamma_i^+ - C_{SS} \gamma_i^-)$$

$$\gamma_i^+ = \sum_{n=k}^{\infty} [(n+1)^i - n^i] \cdot \lambda_n \hat{f}_n$$

$$\gamma_i^- = \sum_{n=k}^{\infty} [n^i - (n+1)^i] \cdot \lambda_n \frac{C_{n+1}^*}{C_{SS}} \hat{f}_{n+1}$$

- Note: Using the definition of moments, these infinite summations can be written in terms of the moments, which is what the model actually computes

$$\hat{f}_n = \frac{f_n}{m_0}$$



# A More Efficient Approach

## Moments

- $m_0$ : Number of precipitates
- $m_1$ : Number of atoms inside precipitates
- $m_2$ : Breadth of distribution
- $m_n$ : Related to shape

$$\frac{\partial C}{\partial t} = \nabla \cdot (D \nabla C) - 2I_1 - Dm_0(C\gamma_1^+ - \gamma_1^-)$$

$$m_i = \sum_{n=k=2} n^i \cdot f(n)$$

$$\frac{\partial m_0}{\partial t} = I_1$$

$$\frac{\partial m_1}{\partial t} = 2I_1 + Dm_0(C\gamma_1^+ - \gamma_1^-)$$

$$\frac{\partial m_2}{\partial t} = 4I_1 + Dm_0(C\gamma_2^+ - \gamma_2^-)$$



# Closure Assumptions

Finite set of moments insufficient to describe a complete distribution. Need a closure assumption to allow  $\gamma$  terms to be written in terms of moments.

## ◆ Delta Function Approximation

- Assumes all precipitates are of average size ( $m_1/m_0$ )
- Still need to estimate distribution for nucleation of smallest precipitate

## ◆ Free energy-minimizing distribution

- Results in a non-linear system of equations that must be solved.
  - ◆ Can be pre-computed and interpolated during the simulation; need  $m_2$ .

## ◆ Other distributions

- Log-normal observed for dislocation loops.
  - ◆ Can be pre-computed. Need  $m_2$  (or model for  $m_2(m_1/m_0)$ ).



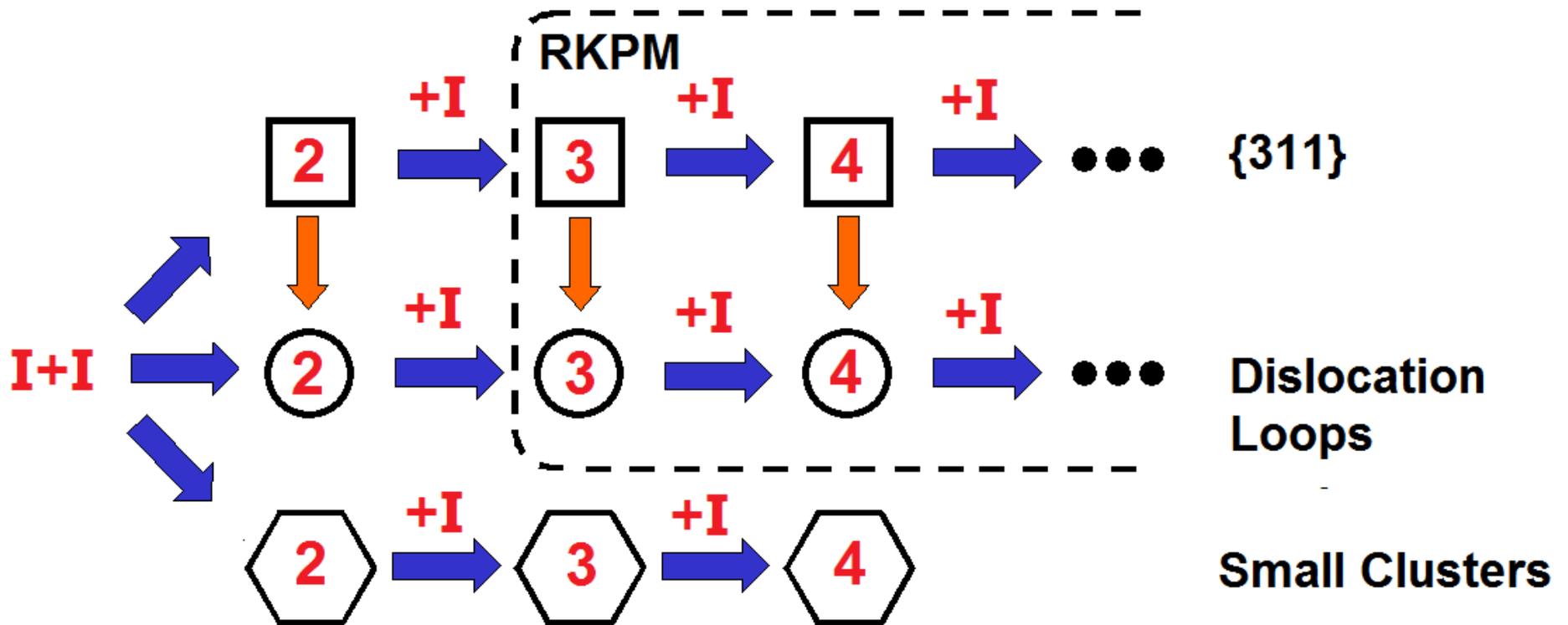
# Outline

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- ◆ Motivation
- ◆ The Problem
- ◆ Modeling of Precipitation
- ◆ Reduced Kinetic Precipitation Model
- ◆ **RKPM Example: Dislocations**
  - Big Picture Overview
  - *Ab Initio* Calculations
  - Stress Effects
  - Loop Energy
  - Results
- ◆ Oxygen Precipitation
- ◆ Proposed Research



# Big Picture Overview

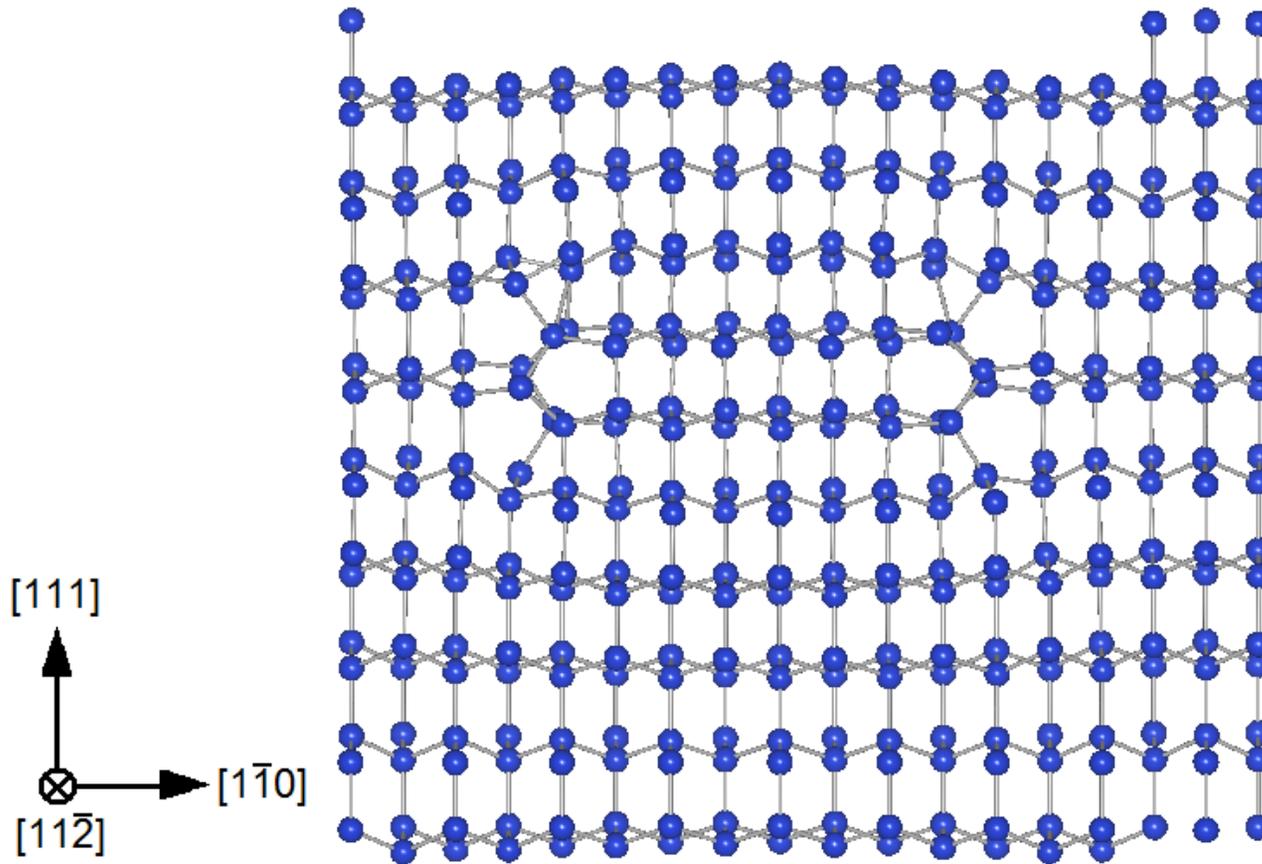


Note: Vacancy interactions omitted for clarity.





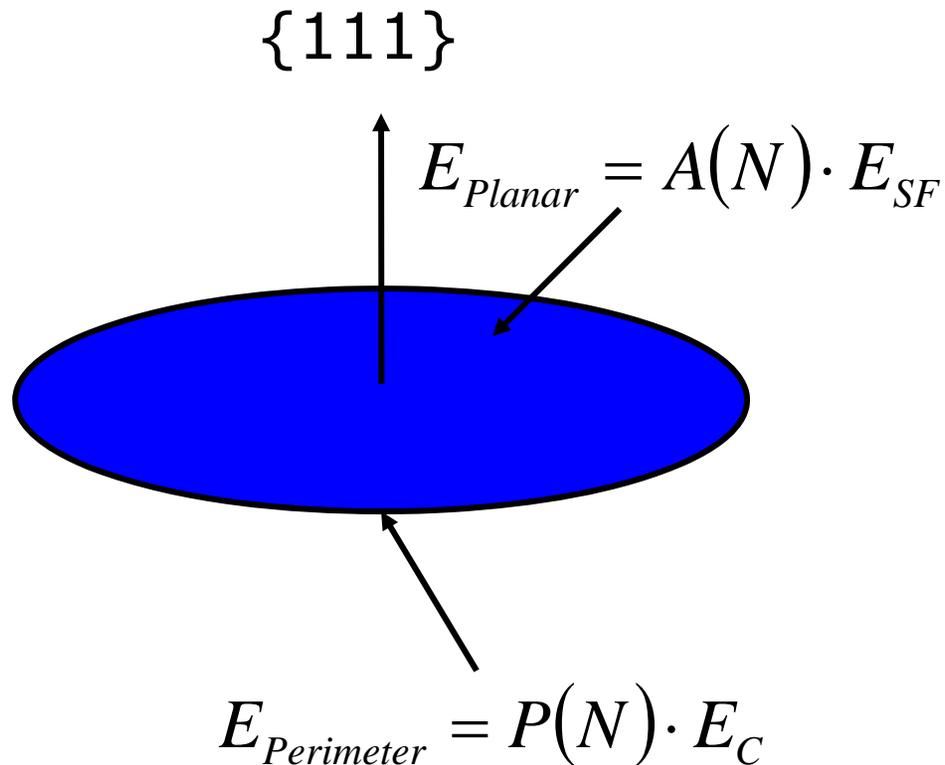
# Dislocation Dipole



Dislocation dipole system.



# Loop Energy



Total formation energy of loop:

$$E_f = E_{Perimeter} + E_{Planar} + E_S$$

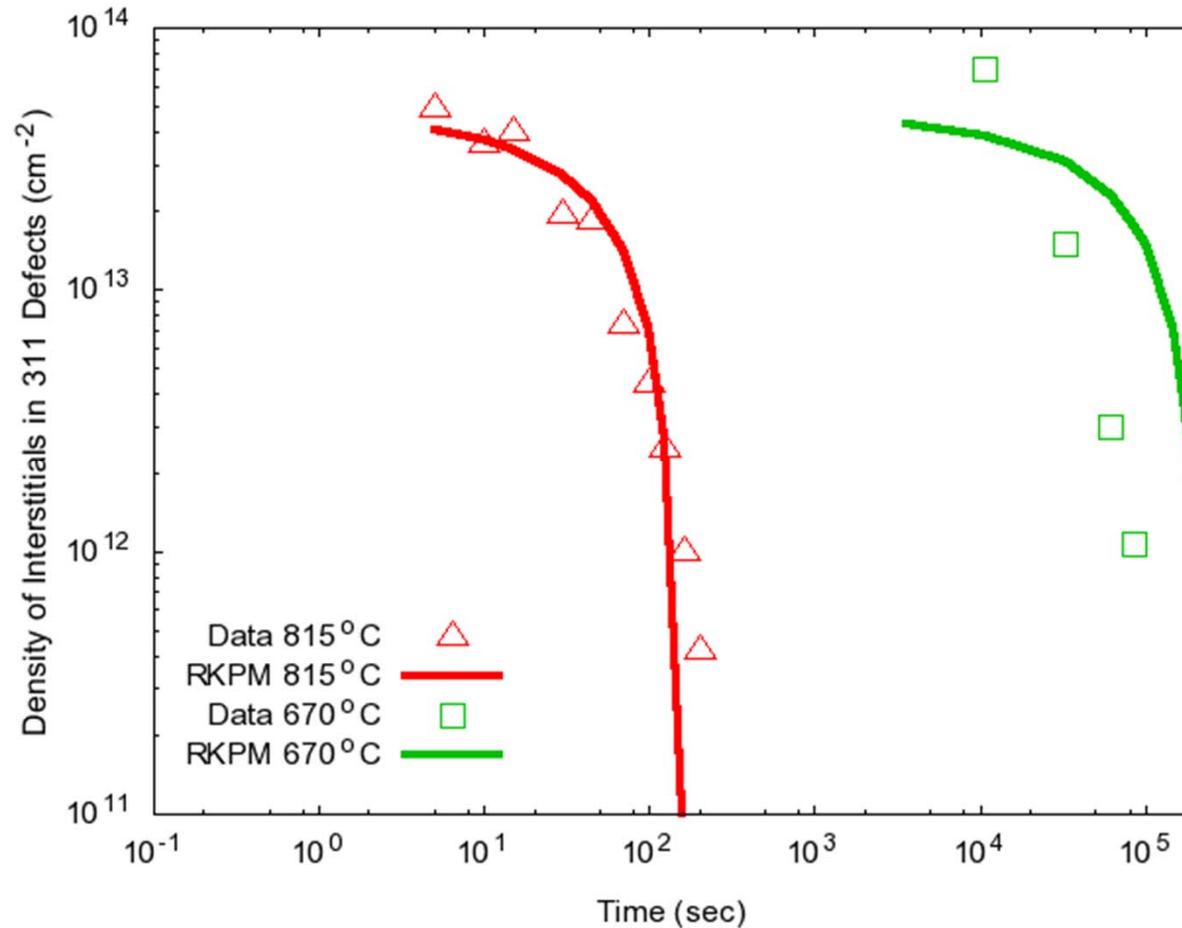
$E_S$  = Elastic self-energy

Change with applied strain:

$$\Delta E_f = -\frac{V}{2} \sum_{i=1}^3 \sum_{j=1}^3 \Delta \varepsilon_{ij} \sigma_{ij}$$



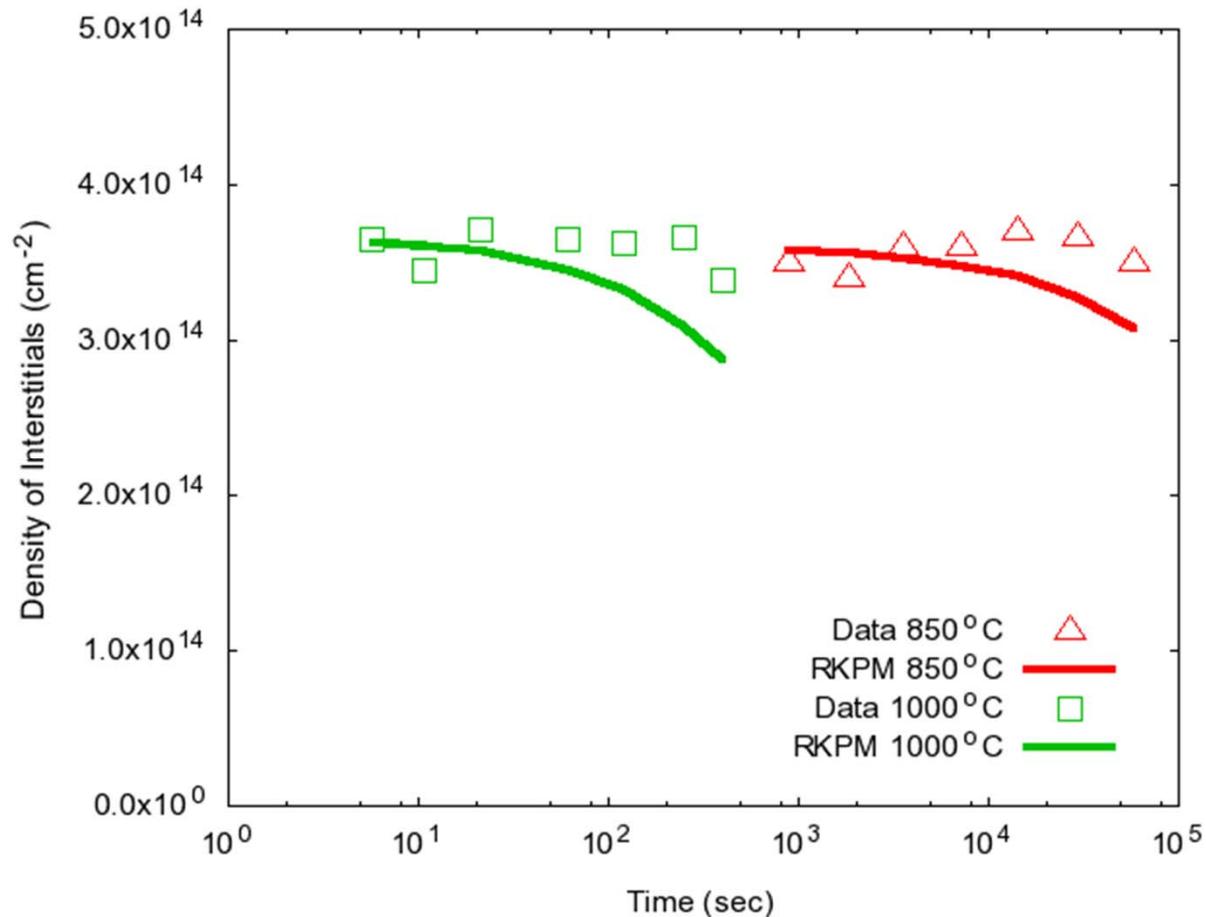
# Results



Density of interstitials bound to {311} defects compared to data (Eaglesham *et al*).



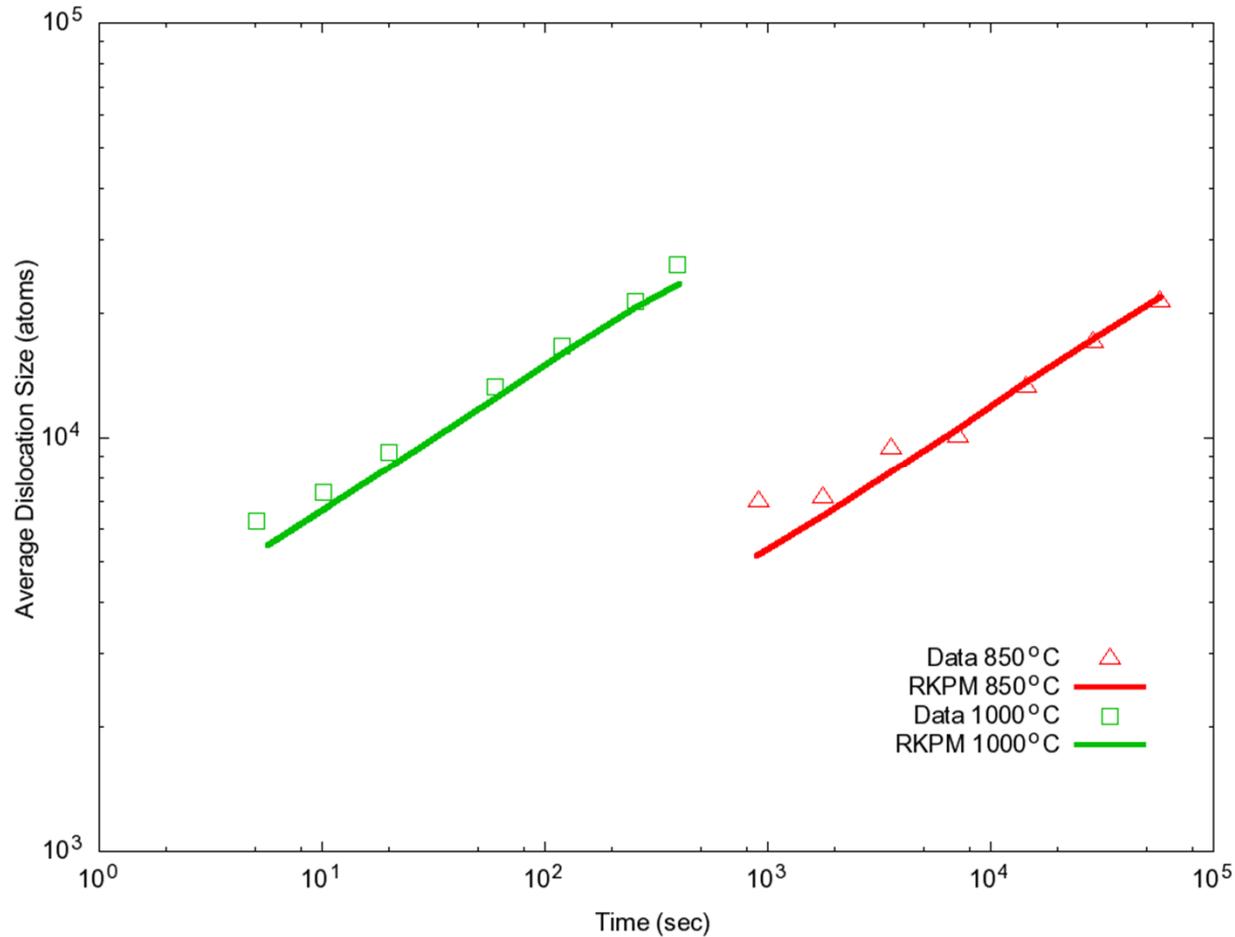
# Results



Density of interstitials bound to dislocation loops compared to data (Pan *et al*).



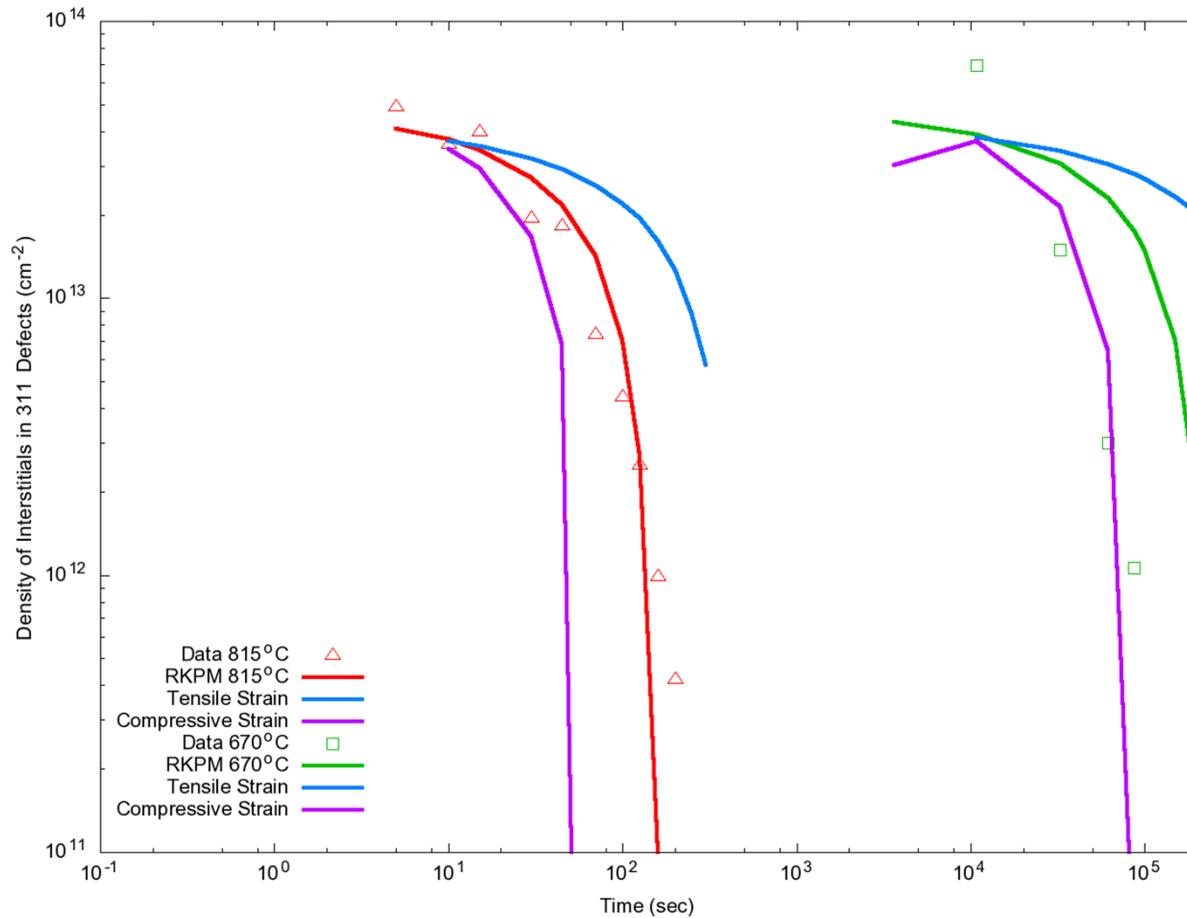
# Results



Growth in average dislocation size over time compared to data (Pan *et al*).



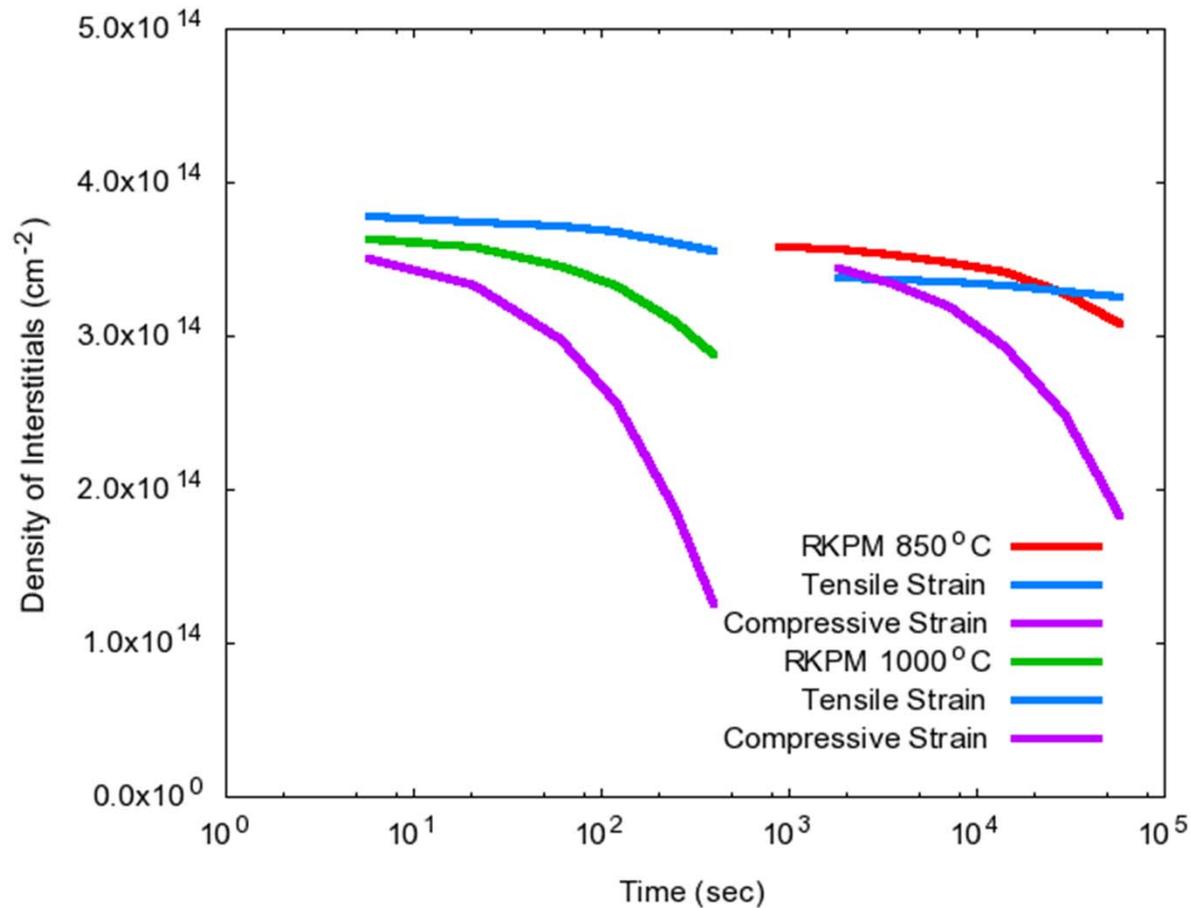
# Results



Impact of 1.5% biaxial strain on {311} defects.



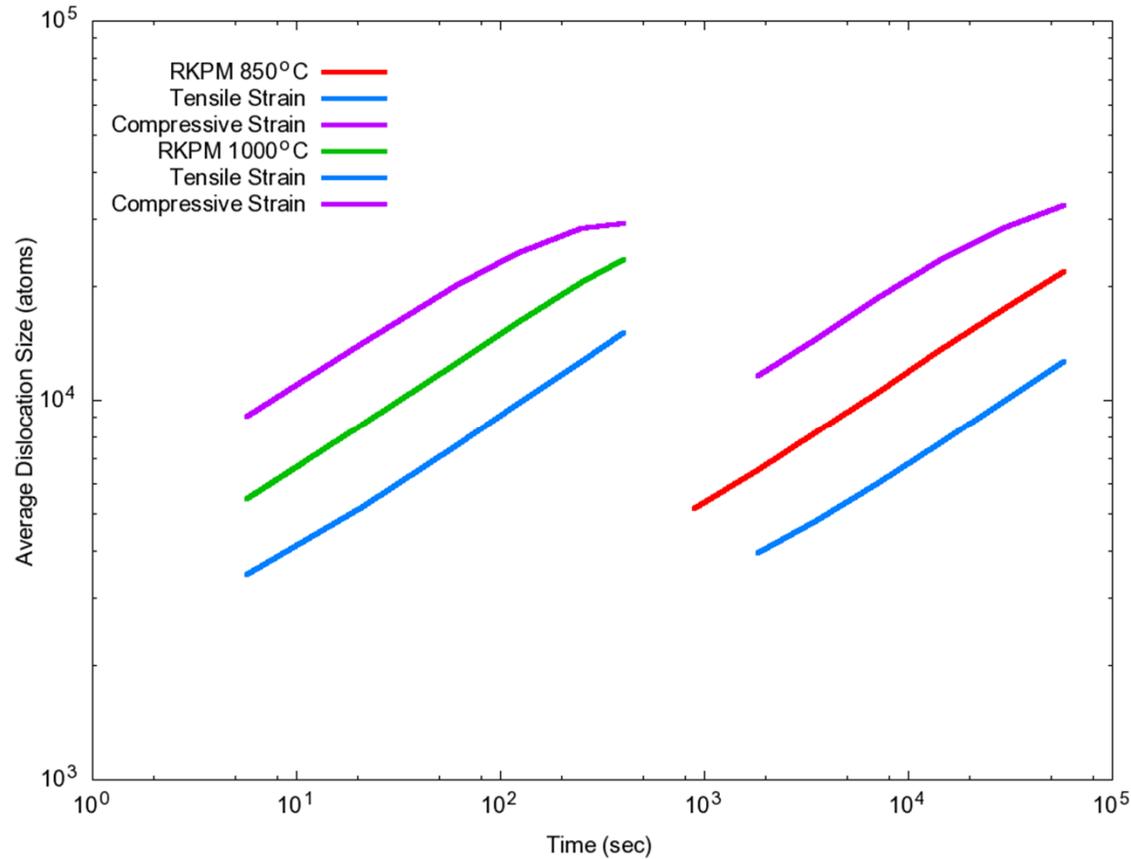
# Results



Impact of 1.5% biaxial strain on dislocation loops.



# Results



Impact of 1.5% biaxial strain on loop growth rates.



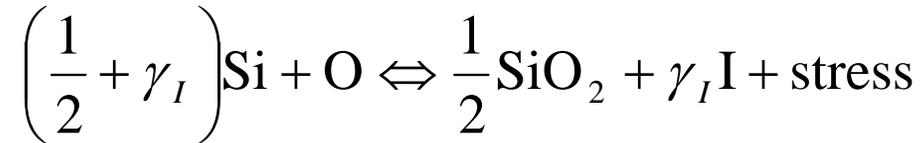
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  - Oxygen Growth/Dissolution Model
  - Oxygen/Silicon Interface
  - Oxygen Data
  - Interaction w/ Dislocation Loops
- ◆ Proposed Research



# Oxygen Growth/Dissolution Model



Energy

$$G_0 = -nk_B T \ln\left(\frac{C_o}{C_o^*}\right)$$

$$G_{if} = 4\pi r^2 \alpha$$

$$G_s = \frac{4}{3} \pi r^3 6\mu_{Si} e_C e_T$$

$$G_i = \gamma_I nk_B T \ln\left(\frac{C_I}{C_I^*}\right)$$

$$G_v = -\gamma_v nk_B T \ln\left(\frac{C_v}{C_v^*}\right)$$

Strain

$$e_T = e_C \left(1 + \frac{4\mu_{Si}}{3K_{SiO_2}}\right)$$

$$e_C = \frac{k_B T}{4\mu_{Si} V_{Si}} \ln\left(\frac{C_I}{C_I^*}\right) + \frac{\alpha}{4\mu_{Si} r_p} \left(1 - \frac{3K_{SiO_2}}{3K_{SiO_2} + 4\mu_{Si}}\right)$$

$$\gamma_I = \frac{1}{2} \left[ \frac{V_{SiO_2}}{V_{Si}} (1 + e_T)^{-3} - 1 \right]$$

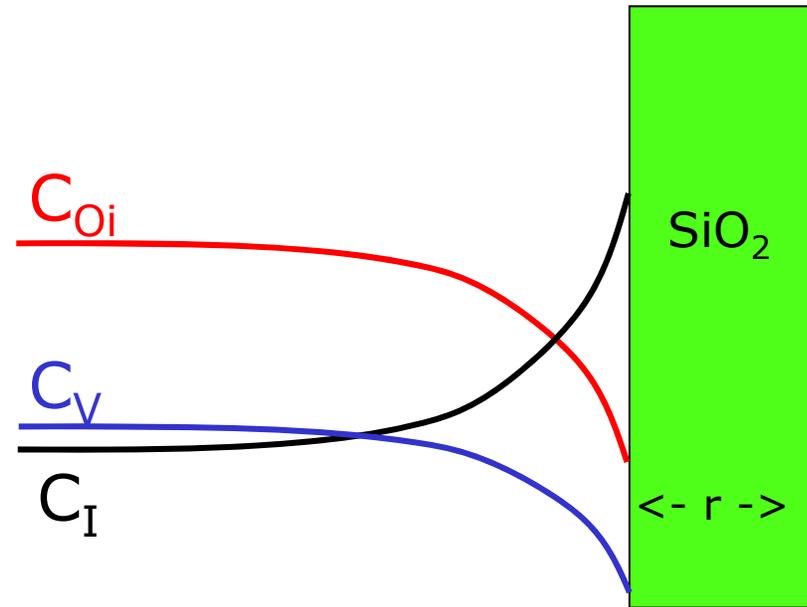
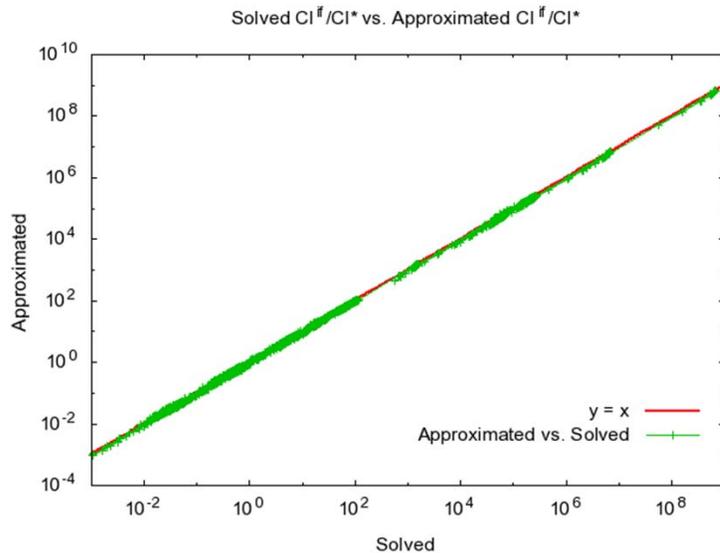


# Oxygen/Silicon Interface

## Interfacial Oxygen, Interstitial Silicon

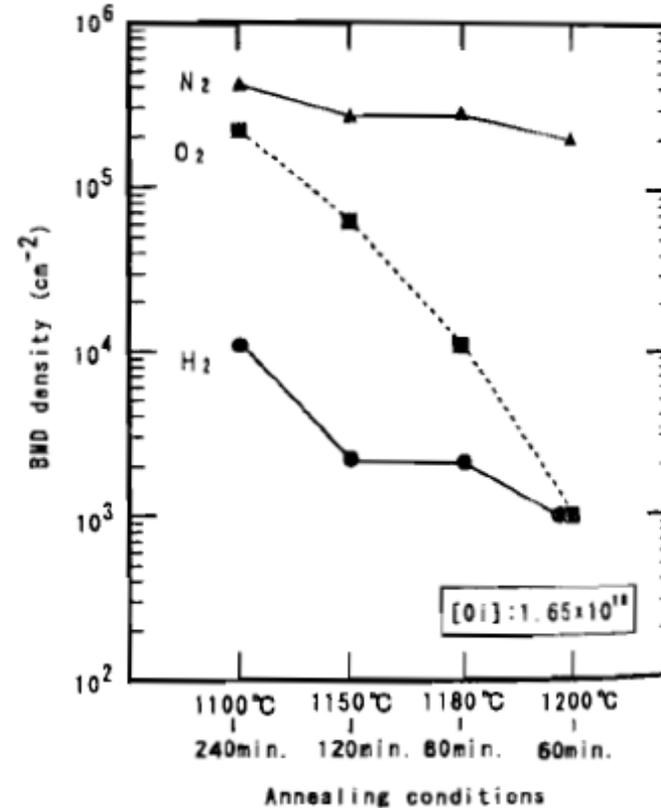
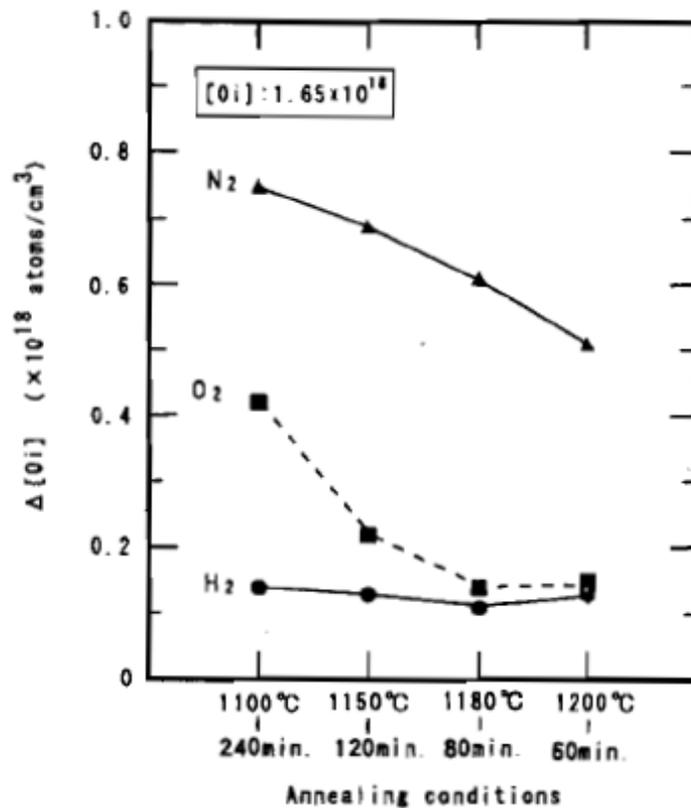
$$D_o \frac{C_o - C_o^{if}}{r} = k_r (C_o^{if} - C_o^*) = \frac{D_I}{\gamma_I} \frac{C_I^{if} - C_I}{r}$$

Result is a transcendental equation. Can approximate numerically.





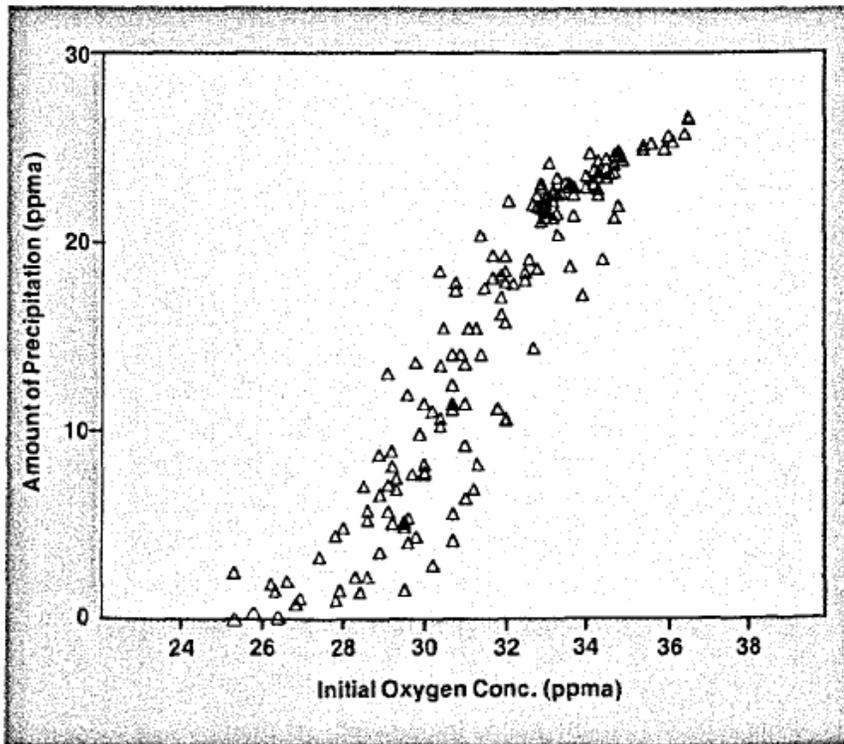
# Oxygen Data



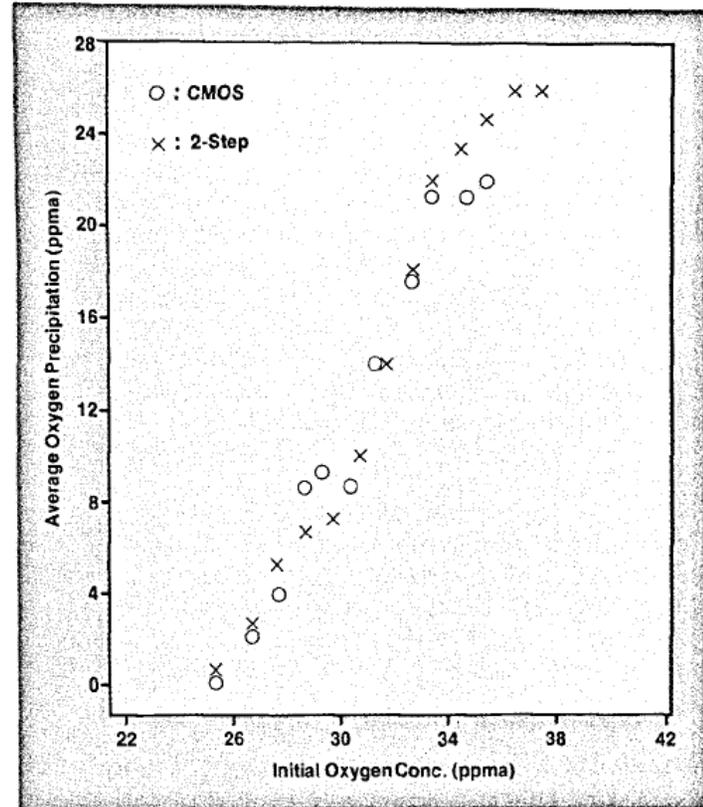
Abe, Suzuki and Koya, *J. Electrochem. Soc.* **144**, 306 (1997)



# Oxygen Data



Series of 800°C/2h + 1050°C/16h



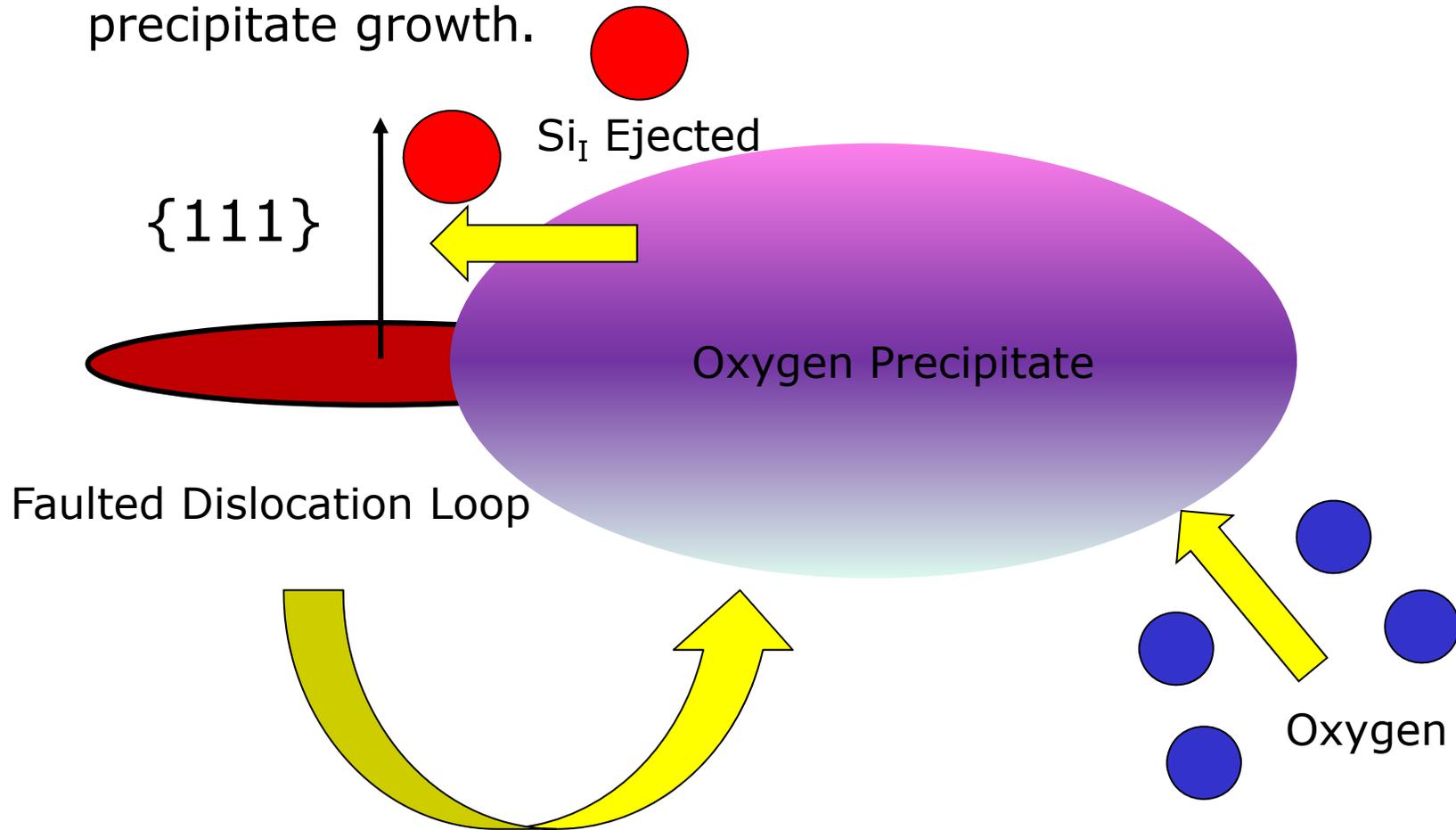
CMOS simulation and 800°C/2h + 1050°C/16h

H-D. Chiou, *Solid State Tech.* **30**, 77 (1987)



# Interaction w/ Dislocation Loops

Faulted dislocation loops generated in regions of high stress and large Si interstitial concentrations. Accelerate precipitate growth.





# Precipitate Energetics

Per-atom free energy of infinitely large precipitate:

$$G_{\infty} = G_P - kT \ln \frac{C}{C_{Si}}$$

Define *solid solubility* as concentration at which  $G_{\infty} = 0$ :

$$C_{SS} = C_{Si} \exp \left\{ \frac{G_P}{kT} \right\}$$

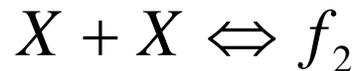
Interpret  $C_{SS}$  as concentration above which precipitates form. For finite precipitates, a surface (excess) energy term is needed:

$$G_n = -n \cdot kT \ln \frac{C}{C_{SS}} + G_{exc}(n)$$

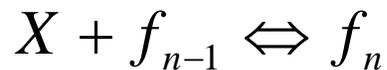


# Precipitate Energetics

Formation and growth reactions:



In equilibrium:



$$f_n^* = K_n \cdot C \cdot f_{n-1}^*$$

Equilibrium concentration of precipitate depends on number of lattice sites it can sit on and energy:

$$f_n^* = C_{Si} \exp\left\{\frac{-G_n}{kT}\right\}$$

$$K_n = \frac{f_n^*}{C \cdot f_{n-1}^*} = \frac{1}{C} \exp\left\{\frac{-(G_n - G_{n-1})}{kT}\right\}$$



# Growth Kinetics

Birth death process of discrete precipitate sizes:

$$\frac{\partial n}{\partial t} = g_{n-1} - d_n$$

$g_n$ : Growth rate,  $n \rightarrow n+1$

$d_n$ : Dissolution rate,  $n \rightarrow n-1$

Flux in size-space from  $n$  to  $n+1$  (ie. concentration of precipitates growing from size  $n$  to  $n+1$ ):

$$R_n = g_n f_n - d_{n+1} f_{n+1}$$

Leading to equation for precipitates of size  $n$ :

$$\frac{\partial f_n}{\partial t} = R_{n-1} - R_n$$