

Solutions

UW ID#:

Average = 25.0
Section: _____ Version A

Std Dev = 8.9

Max = 43, Min = 8

Exam 3 — EE 233

Fall 2011

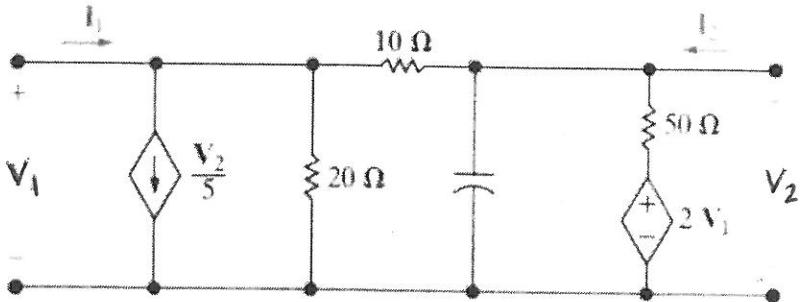
The test is closed book, with one sheet of notes and standard calculators (no communications) allowed. Show all work. Be sure to state all assumptions made and check them when possible. The number of points per problem are indicated in parentheses. Total of 50 points in 3 problems on 3 pages.

1. In the circuit at right, v_1 is the input and v_2 is the output. $C = 20 \text{ mF}$.

- (a) Calculate the impulse response. (7)

$$KCL @ V_2:$$

$$\frac{V_2 - V_1}{10} + \frac{V_2}{1/SC} + \frac{V_2 - 2V_1}{50} = 0$$



$$V_2 \left[\frac{1}{10} + SC + \frac{1}{50} \right] = V_1 \left[\frac{1}{10} + \frac{2}{50} \right] \Rightarrow \frac{V_2}{V_1} = H(s) = \frac{7}{6 + 50Cs} = \frac{7}{6 + s}$$

$$h(t) = \mathcal{L}^{-1}\{H(s)\} = \underline{7e^{-6t}u(t)}$$

- (b) Determine $v_2(t)$ for $v_1(t) = 6e^{-4t}u(t)$. (10)

$$v_2(t) = v_1(t) * h(t) = \int_{-\infty}^{\infty} h(\lambda) v_1(t-\lambda) d\lambda = \int_{-\infty}^{\infty} 7e^{-6\lambda} u(\lambda) 6e^{-4(t-\lambda)} u(t-\lambda) d\lambda$$

$$= \int_0^t 42 e^{-6\lambda} e^{-4t} e^{4\lambda} d\lambda \quad \text{for } t > 0, = 0 \text{ otherwise}$$

$$= 42 e^{-4t} u(t) \int_0^t e^{-2\lambda} d\lambda = 42 e^{-4t} u(t) \left[\frac{e^{-2\lambda}}{-2} \right]_0^t = -21 e^{-4t} (e^{-2t} - 1) u(t)$$

$$v_2(t) = \underline{21(e^{-6t} - e^{-4t}) u(t)}$$

$$v_2(t) = \mathcal{L}^{-1}[V_1(s)H(s)] \quad V_1(s)H(s) = \left(\frac{6}{s+4} \right) \left(\frac{7}{s+6} \right) = \frac{K_1}{s+4} + \frac{K_2}{s+6}$$

$$K_1 = \frac{6 \times 7}{s+6} \Big|_{s=4} = 21 \quad K_2 = \frac{6 \times 7}{s+4} \Big|_{s=-6} = -21$$

$$v_2(t) = \underline{(21e^{-4t} - 21e^{-6t}) u(t)}$$

Solutions

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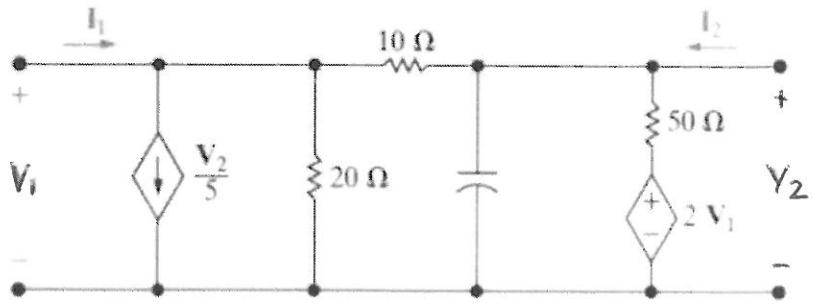
The test is closed book, with one sheet of notes and standard calculators (no communications) allowed. Show all work. Be sure to state all assumptions made and check them when possible. The number of points per problem are indicated in parentheses. Total of 50 points in 3 problems on 3 pages.

1. In the circuit at right, v_1 is the input and v_2 is the output. $C = 5 \text{ mF}$.

- (a) Calculate the impulse response. (7)

KCL @ V_2 :

$$\frac{V_2 - V_1}{10\Omega} + \frac{V_2}{1/SC} + \frac{V_2 - 2V_1}{50\Omega} = 0$$



$$V_2 \left[\frac{1}{10} + \frac{1}{50} + SC \right] = V_1 \left[\frac{1}{10} + \frac{2}{50} \right] \Rightarrow \frac{V_2}{V_1} = H(s) = \frac{\frac{7}{6+0.250s}}{24+s}$$

$$\mathcal{L} \left\{ \frac{28}{5+24} \right\} = 28e^{-24t} u(t) = h(t)$$

- (b) Determine $v_2(t)$ for $v_1(t) = 12e^{-10t}u(t)$. (10)

$$v_2(t) = v_1(t) * h(t) = \int_{-\infty}^{\infty} h(\lambda) v_1(\lambda-t) d\lambda = \int_{-\infty}^{\infty} 28e^{-24\lambda} u(\lambda) 12e^{-10(t-\lambda)} u(t-\lambda) d\lambda$$

$$= \int_0^t (28 * 12) e^{-24\lambda} e^{-10t} e^{10\lambda} d\lambda \quad \text{for } t > 0$$

$$= u(t) 336 e^{-10t} \int_0^t e^{-14x} dx = 336 e^{-10t} \left[\frac{e^{-14x}}{-14} \right]_0^t = -24 e^{-10t} [e^{-14t} - 1]$$

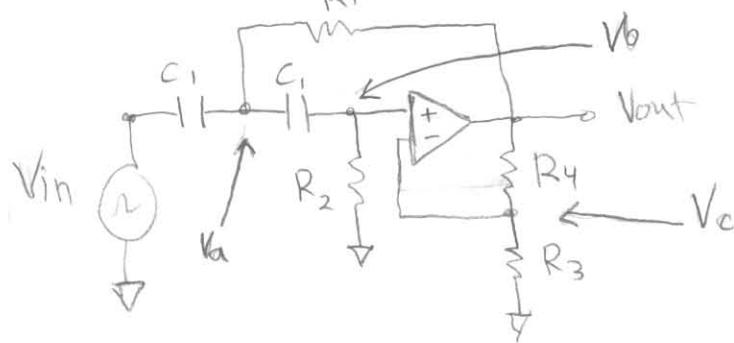
$$v_2(t) = \underline{24 [e^{-10t} - e^{-24t}] u(t)}$$

$$v_2(t) = f^{-1} \{ V_1(s) H(s) \} = f^{-1} \left\{ \frac{12 \cdot 28}{(s+10)(s+24)} \right\} = 2 \left\{ \frac{K_1}{s+10} + \frac{K_2}{s+24} \right\}$$

$$K_1 = \frac{12 * 28}{s+24} \Big|_{s=-10} = 24 \quad K_2 = \frac{12 * 28}{s+10} \Big|_{s=-24} = -24$$

$$v_2(t) = \underline{[24e^{-10t} - 24e^{-24t}] u(t)}$$

Problem 2 solution



①

Nodal equation at V_a

$$\frac{V_a - V_{in}}{\frac{1}{SC_1}} + \frac{V_a - V_b}{\frac{1}{SC_1}} + \frac{V_a - V_{out}}{R_1} = 0$$

$$(V_a - V_{in})SC_1 + (V_a - V_b)SC_1 + \frac{V_a - V_{out}}{R_1} = 0$$

$$V_a(SC_1 + SC_1 + \frac{1}{R_1}) - V_{in}SC_1 - V_bSC_1 - \frac{V_{out}}{R_1} = 0$$

$$V_a(2SC_1 + \frac{1}{R_1}) - V_bSC_1 - \frac{V_{out}}{R_1} = V_{in}SC_1$$

②

Nodal equation at V_b

$$\frac{V_b - V_a}{\frac{1}{SC_1}} + \frac{V_b}{R_2} = 0$$

$$V_bSC_1 - V_aSC_1 + \frac{V_b}{R_2} = 0$$

$$V_b(SC_1 + \frac{1}{R_2}) = V_aSC_1$$

$$V_b(1 + \frac{1}{SC_1R_2}) = V_a$$

(3) Nodal equation at V_c

$$\frac{V_c - V_{out}}{R_4} + \frac{V_c}{R_3} = 0$$

$$V_c(\frac{1}{R_4} + \frac{1}{R_3}) = \frac{V_{out}}{R_4}$$

$$V_c(\frac{R_3}{R_4R_3} + \frac{R_4}{R_4R_3}) = \frac{V_{out}}{R_4}$$

$$V_c(\frac{R_4 + R_3}{R_4R_3}) = \frac{V_{out}}{R_4}$$

$$V_c = \frac{R_3}{R_4 + R_3} V_{out}$$

$$V_c = V_b \text{ so } V_a = V_{out} \left(\frac{R_3}{R_4 + R_3} \right) \left(1 + \frac{1}{SC_1 R_2} \right), \text{ plugging back}$$

$$V_{out} \left(\frac{R_3}{R_4 + R_3} \right) \left(1 + \frac{1}{SC_1 R_2} \right) \left(2SC_1 + \frac{1}{R_1} \right) - \left(\frac{R_3}{R_4 + R_3} \right) (V_{out})SC_1 - \frac{V_{out}}{R_1} = V_{in}SC_1$$

$$V_{out} \left[\left(\frac{R_3}{R_4+R_3} \right) \left(1 + \frac{1}{SC_1 R_2} \right) \left(2SC_1 + \frac{1}{R_2} \right) - \frac{R_3}{R_4+R_3} SC_1 - \frac{1}{R_1} \right] = V_{in} SC_1$$

multiply by $SC_1 R_2 R_1$

$$V_{out} \left[\left(\frac{R_3}{R_4+R_3} \right) (SC_1 R_2 R_1 + R_1) \left(2SC_1 + \frac{1}{R_2} \right) - \left(\frac{R_3}{R_4+R_3} \right)^2 SC_1^2 R_2 R_1 - SC_1 R_2 \right]$$

$$= V_{in} S^2 C_1^2 R_1 R_2$$

$$= V_{out} \left(\frac{R_3}{R_4+R_3} \right) \left[(SC_1 R_2 R_1 + R_1) \left(2SC_1 + \frac{1}{R_2} \right) - S^2 C_1^2 R_1 R_2 - \left(\frac{R_4+R_3}{R_3} \right) SC_1 R_2 \right]$$

$$= V_{out} \left(\frac{R_3}{R_4+R_3} \right) \left[2S^2 C_1^2 R_2 R_1 + SC_1 R_1 + 2SC_1 R_1 + 1 - S^2 C_1^2 R_1 R_2 - \frac{R_4+R_3}{R_3} SC_1 R_2 \right]$$

$$= V_{out} \left(\frac{R_3}{R_4+R_3} \right) \left[S^2 C_1^2 R_1 R_2 + S(C_1 R_1 + 2C_1 R_1 + \frac{R_4+R_3}{R_3} C_1 R_2) + 1 \right]$$

$$= V_{out} \left(\frac{R_3}{R_4+R_3} \right) \left[S^2 C_1^2 R_1 R_2 + S(3C_1 R_1 - C_1 R_1 - \frac{R_4}{R_3} C_1 R_1) + 1 \right]$$

$$= V_{out} \left(\frac{R_3}{R_4+R_3} \right) \left[S^2 C_1^2 R_1 R_2 + S(2C_1 R_1 - \frac{R_4}{R_3} C_1 R_1) + 1 \right]$$

so $\frac{V_{out}}{V_{in}} = \frac{R_4+R_3}{R_3} \left[\frac{S^2 C_1^2 R_1 R_2}{S^2 C_1^2 R_1 R_2 + S(2C_1 R_1 - \frac{R_4}{R_3} C_1 R_1) + 1} \right]$

this is a high pass filter

$$|H(s)|_{s \rightarrow 0} = 0$$

$$|H(s)|_{s \rightarrow \infty} = \frac{R_4+R_3}{R_3}$$

Solution Problem 3

$$a) H(s) = \frac{-\frac{R_2}{R_1} s^2}{s^2 + \frac{s}{R_1 C_1} + \frac{1}{R_1 R_2 C_1 C_2}}$$

conditions: Corner frequency: ω_0 rad/s

passband gain: G_1 dB

gain at the corner frequency: G_2 dB

use CnF capacitor when necessary

$$H(s) = \frac{K s^2}{s^2 + \beta s + \omega_0^2} \Rightarrow \text{passband gain} = K = 10^{(\frac{G_1}{20})}$$

General 2nd order HPF

Gain at the corner frequency will define Q

at corner frequency, you got a drop of $G_1 - G_2$

$$\text{then } Q = 10^{(-\frac{(G_1 - G_2)}{20})} \quad \begin{matrix} \leftarrow \\ \text{negative sign because} \\ \text{you have a drop} \end{matrix}$$

$$\text{then } Q = \frac{\omega_0}{\beta} \Rightarrow \beta = \frac{\omega_0}{Q}$$

\therefore you are going to have: (1) $\beta = \frac{1}{R_1 C_1} \rightarrow$ solve for R_1

$$(2) K = \frac{R_2}{R_1} \rightarrow \text{solve for } R_2$$

$$(3) \omega_0^2 = \frac{1}{R_1 R_2 C_1 C_2} \rightarrow \text{solve for } C_2$$

3 eqns, 4 unknowns, so let $C_1 = \text{cap value that is suggested above}$

Version A

$$\omega_0 = 20,000 \text{ rad/s} \quad R_1 = 2500 \Omega$$

$$G_1 = 38 \text{ dB} \quad \Rightarrow \quad R_2 = 200k\Omega$$

$$G_2 = 26 \text{ dB} \quad C_2 = 1 \text{nF}$$

$$C_1 = 5 \text{nF}$$

Version B

$$\omega_0 = 50,000 \text{ rad/s} \quad R_1 = 2000 \Omega$$

$$G_1 = 46 \text{ dB} \quad \Rightarrow \quad R_2 = 400k\Omega$$

$$G_2 = 32 \text{ dB} \quad C_2 = 0.25 \text{nF}$$

$$C_1 = 2 \text{nF}$$

b) cutoff frequency:

$$|H(j\omega)| = \frac{|H_{\max}|}{\sqrt{2}}$$

$$\left| \frac{-K(j\omega_c)^2}{(j\omega_c)^2 + \beta j\omega_c + (\omega_0)^2} \right| = \frac{K}{\sqrt{2}} \quad \text{your maximum gain is your passband gain}$$

$$\left| \frac{-\omega_c^2}{(\omega_0^2 - \omega_c^2) + j\beta\omega_c} \right| = \frac{1}{\sqrt{2}}$$

$$\frac{\omega_c^2}{\sqrt{(\omega_0^2 - \omega_c^2)^2 + (\beta\omega_c)^2}} = \frac{1}{\sqrt{2}} \Rightarrow \frac{1}{\sqrt{(\omega_0^2 - \omega_c^2)^2 + (\beta\omega_c)^2}} = \frac{1}{\omega_c^2 \sqrt{2}}$$

equate the denominator²

$$\Rightarrow (\omega_0^2 - \omega_c^2)^2 + \beta^2 \omega_c^2 = 2\omega_c^4$$

$$\omega_0^4 - 2\omega_0^2 \omega_c^2 + \omega_c^4 + \beta^2 \omega_c^2 = 2\omega_c^4$$

$$\omega_c^4 + (2\omega_0^2 - \beta^2)\omega_c^2 - \omega_0^4 = 0$$

$$\omega_c^2 = \frac{-(2\omega_0^2 - \beta^2) \pm \sqrt{(2\omega_0^2 - \beta^2)^2 - 4(1)(-\omega_0^4)}}{2} \quad (\text{Quadratic equation})$$

↳ only have 1 solution, because the second one is negative.

Version A

$$\omega_c = \sqrt{\frac{-(2 \cdot 20,000^2) - 80,000^2 + \sqrt{(2 \cdot 20,000^2 - 80,000^2)^2 - 4 \cdot -(20,000)^4}}{2}}$$

$$= 74.8 \text{ kHz} \approx 75 \text{ kHz}$$

Version B

$$\omega_c = \sqrt{\frac{-(2 \cdot 50,000^2) - 250,000^2 + \sqrt{(2 \cdot 50,000^2 - 250,000^2)^2 - 4 \cdot -(50,000)^4}}{2}}$$

$$\approx 240 \text{ kHz}$$