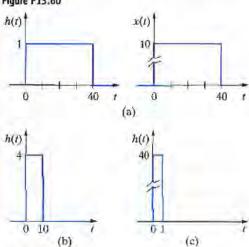
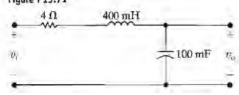
- **13.60** a) Given y(t) = h(t) * x(t), find y(t) when h(t) and x(t) are the rectangular pulses shown in Fig. P13.60(a).
 - Repeat (a) when h(t) changes to the rectangular pulse shown in Fig. P13.60(b).
 - Repeat (a) when h(t) changes to the rectangular pulse shown in Fig. P13.60(c).
 - d) Sketch y(t) versus t for (a)-(c) on a single graph.
 - e) Do the sketches in (d) make sense? Explain.

Figure P13.60



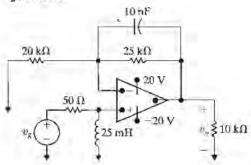
- 13.71 The input voltage in the circuit seen in Fig. P13.71 is $v_i = 10[u(t) u(t 0.1)] \text{ V}.$
 - a) Use the convolution integral to find vo
 - b) Sketch v_o for $0 \le t \le 1$ s.

Figure P13.71



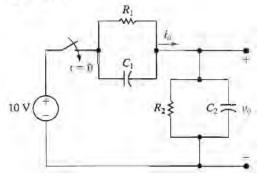
- 13.76 The op amp in the circuit seen in Fig. P13.78 is ideal.
 - a) Find the transfer function $V_o/V_{\rm g}$
 - b) Find v_a if $v_a = 10u(t)$ V.
 - c) Find the steady-state expression for v_0 if $v_g = 8\cos 2000t \text{ V}$.
 - d) Check your answer to (c) with PSpice.

Figure P13.76



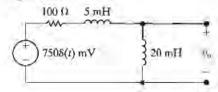
- 13.79 The parallel combination of R_2 and C_2 in the circuit shown in Fig. P13.79 represents the input circuit to a cathode-ray oscilloscope (CRO). The parallel combination of R_1 and C_1 is a circuit model of a compensating lead that is used to connect the CRO to the source. There is no energy stored in C_1 or C_2 at the time when the 10 V source is connected to the CRO via the compensating lead. The circuit values are $C_1 = 5 \text{ pF}$, $C_2 = 20 \text{ pF}$, $R_1 = 1 \text{ M}\Omega$, and $R_2 = 4 \text{ M}\Omega$.
 - a) Find vo.
 - b) Find to.
 - c) Repeat (a) and (b) given C₁ is changed to 80 pF.

Figure P13.79



- 13.85 There is no energy stored in the circuit in Fig. P13.85 at the time the impulsive voltage is applied.
 - a) Find $v_o(t)$ for $t \ge 0$.
 - b) Does your solution make sense in terms of known circuit behavior? Explain.

Figure P13.85



- 14.5 A resistor denoted as R_L is connected in parallel with the capacitor in the circuit in Fig. 14.7. The loaded low-pass filter circuit is shown in Fig. P14.5.
 - a) Derive the expression for the voltage transfer function V₀/V_t.
 - b) At what frequency will the magnitude of H(jω) be maximum?
 - c) What is the maximum value of the magnitude of H(jω)?
 - d) At what frequency will the magnitude of $H(j\omega)$ equal its maximum value divided by $\sqrt{2}$?
 - e) Assume a resistance of 300 kΩ is added in parallel with the 4 nF capacitor in the circuit in Fig. P14.4. Find ω_c, H(j0), H(jω_c), H(j0.2ω_c), and H(j8ω_c).

Figure P14.5

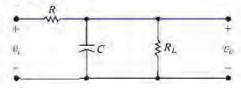
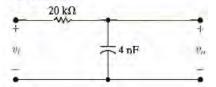


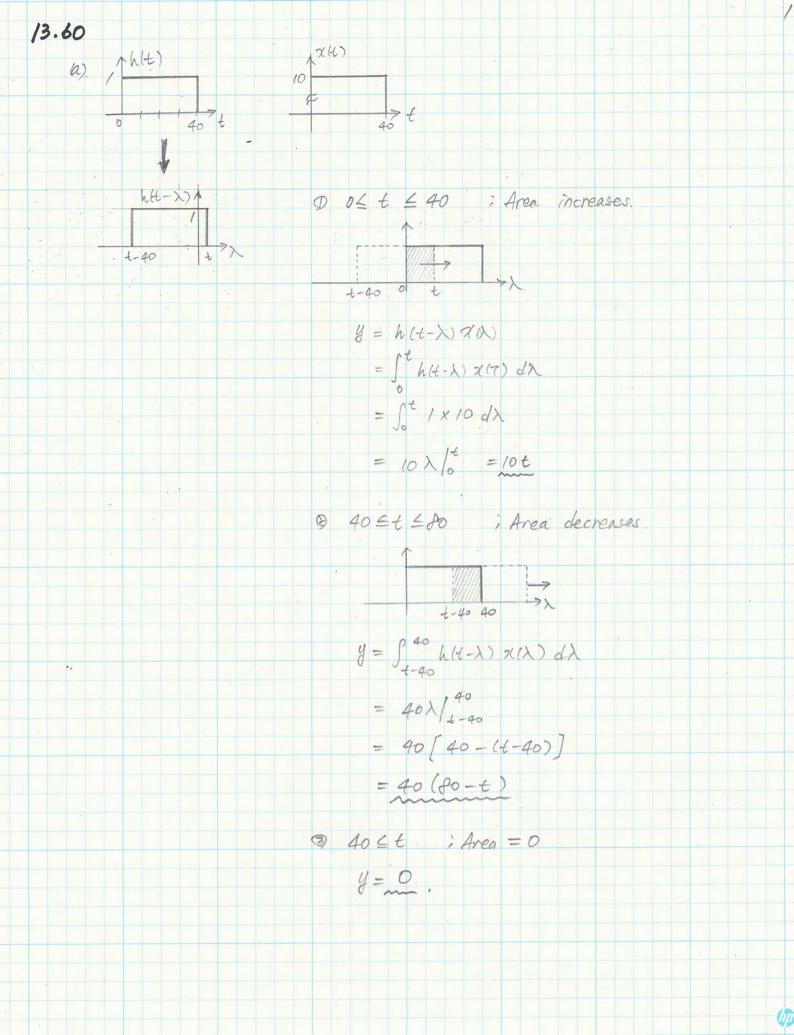
Figure P14.4

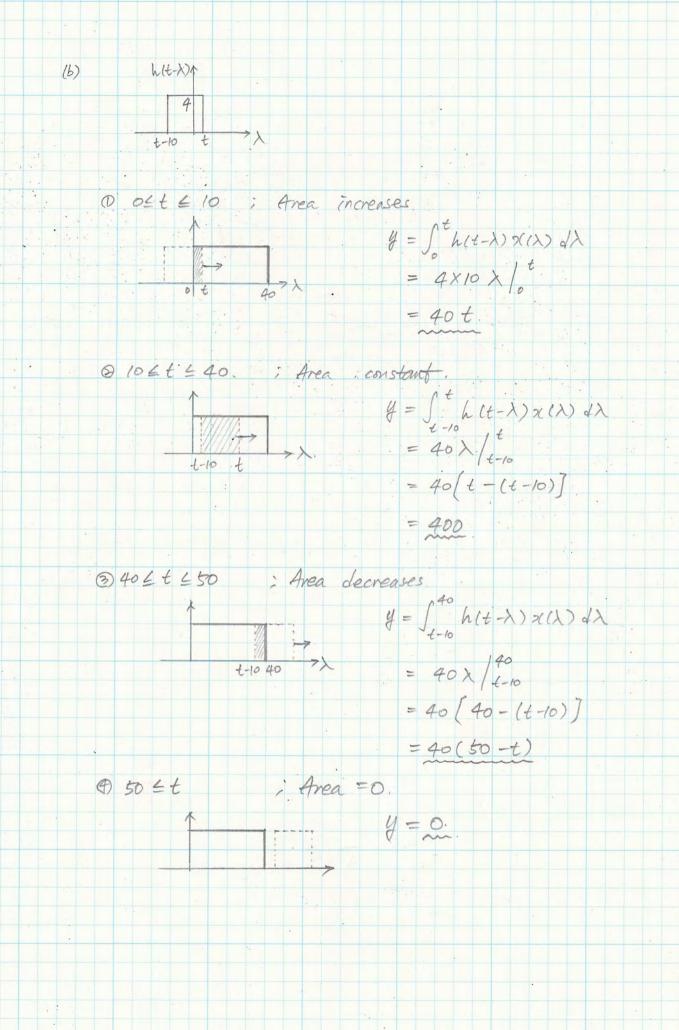


- 14.13 Using a 25 mH inductor, design a high-pass, RL, passive filter with a cutoff frequency of 160 krad/s.
 - a) Specify the value of the resistance.

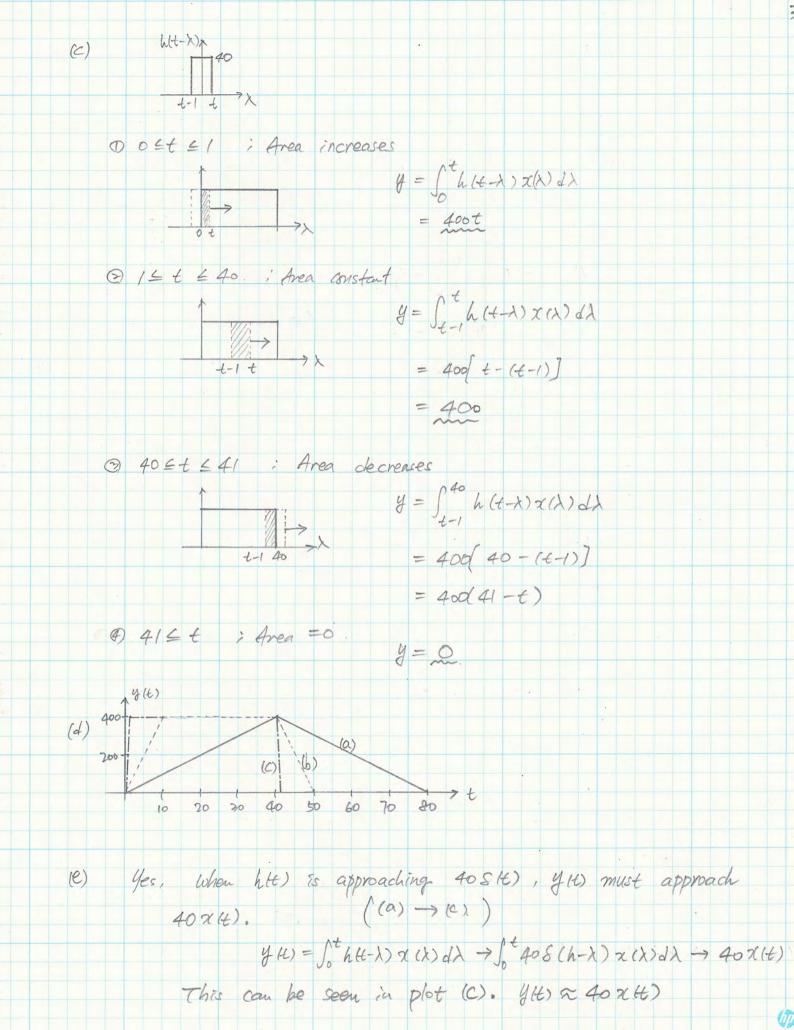
PSPICE

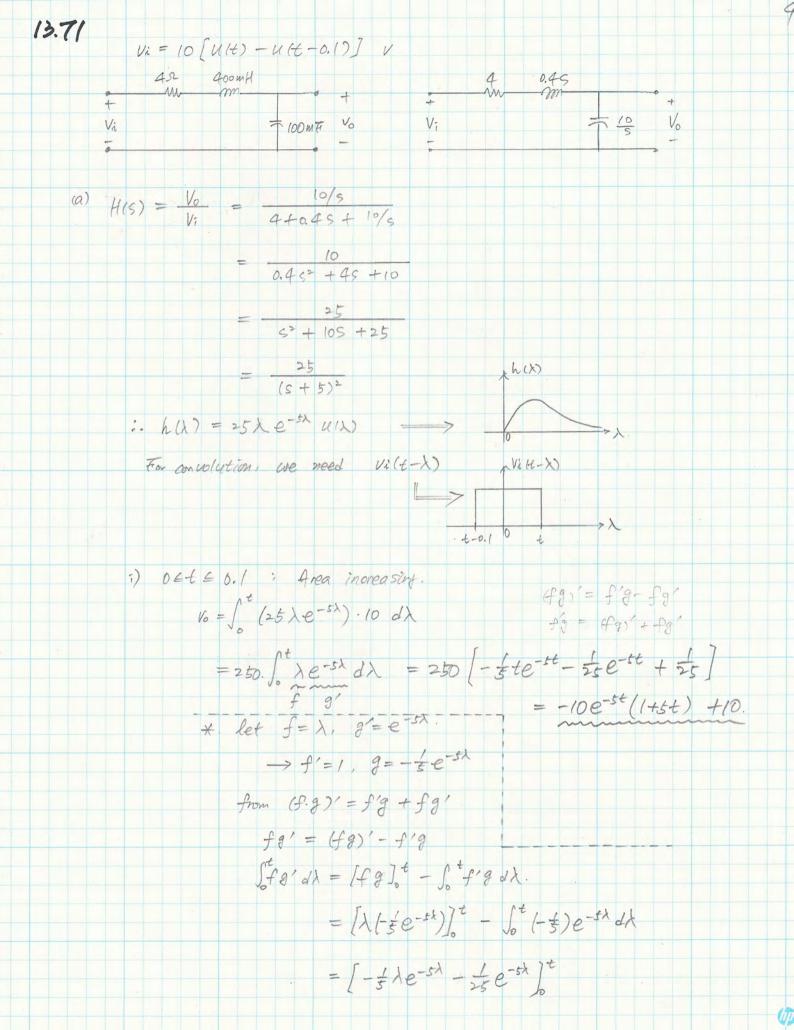
b) Assume the filter is connected to a pure resistive load. The cutoff frequency is not to drop below 150 krad/s. What is the smallest load resistor that can be connected across the output terminals of the filter?

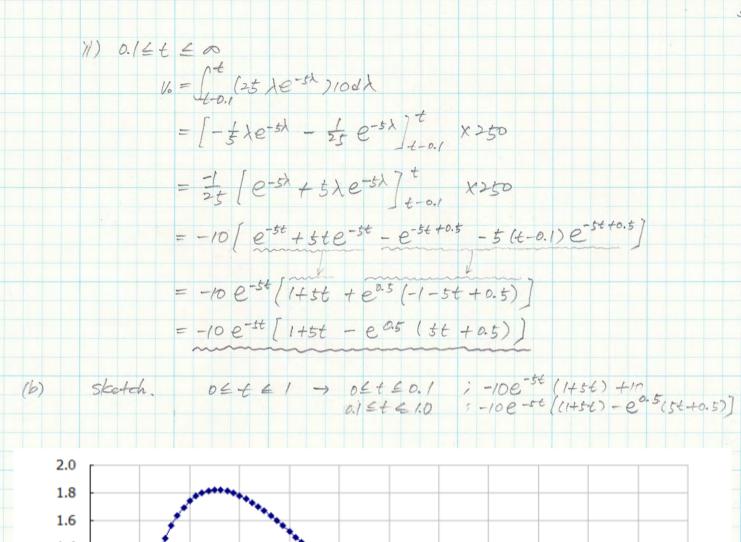


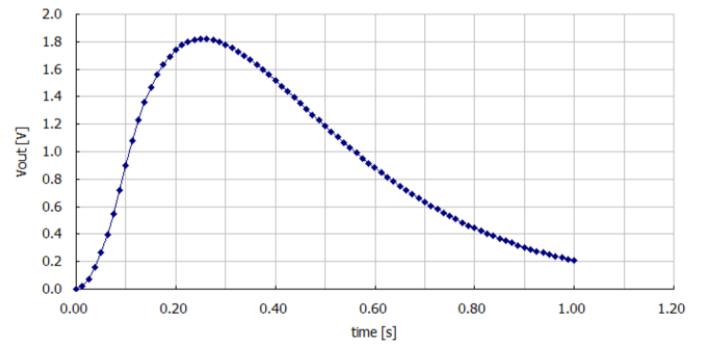


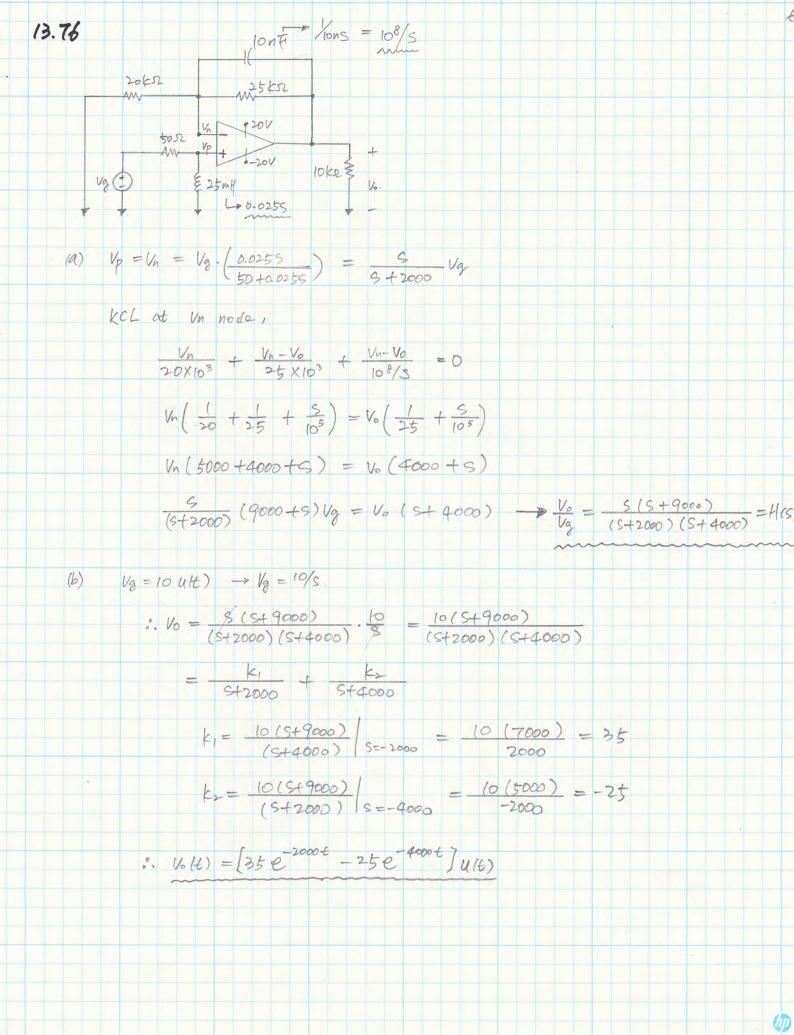
(1)



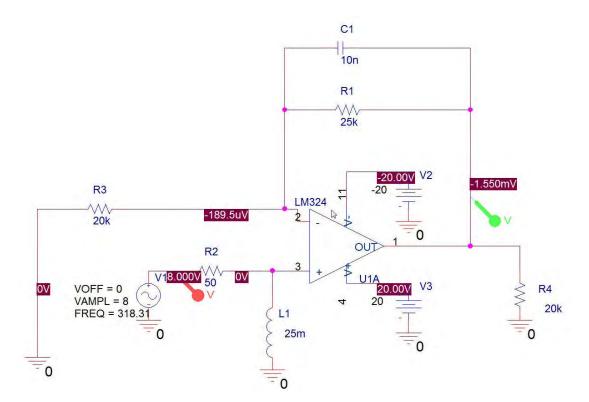


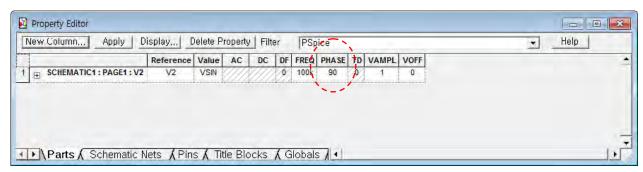


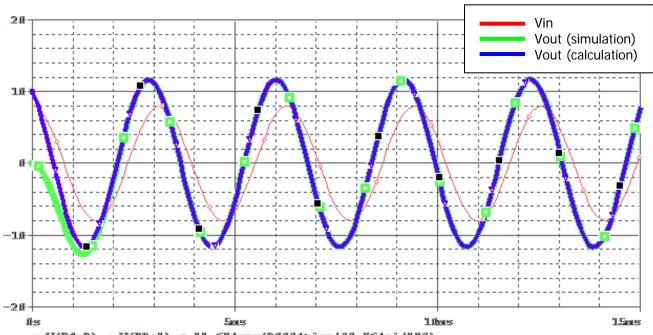


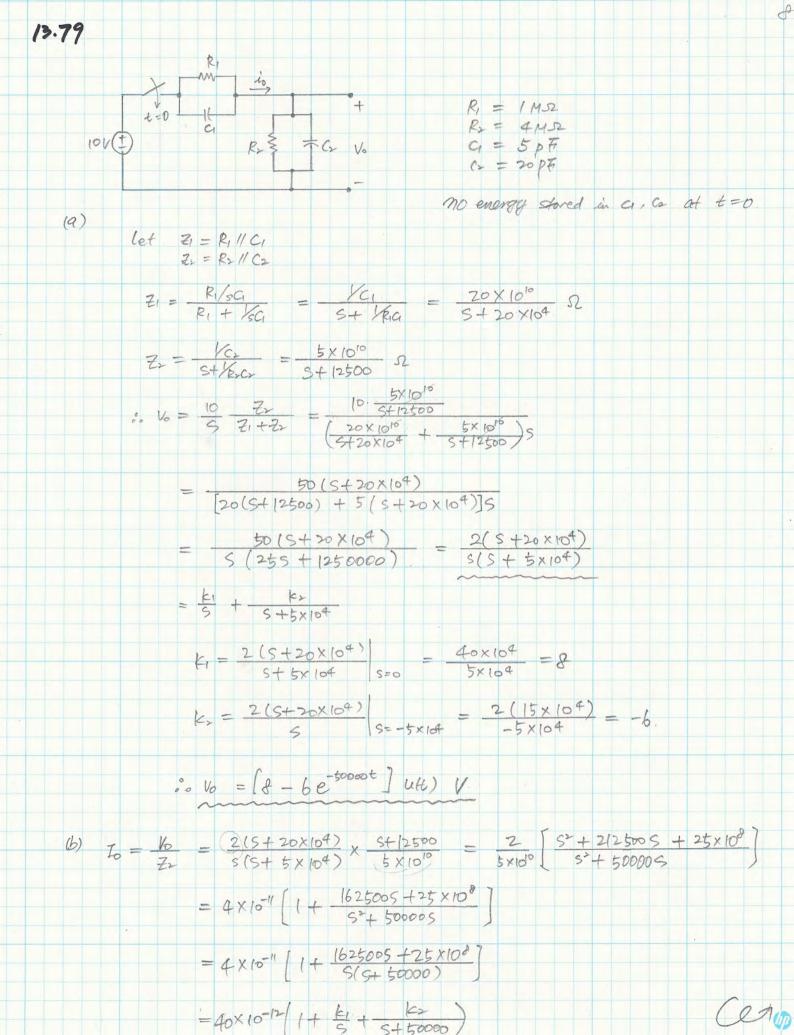


Vg = 8 cos 2000t (C) S=1W=12000 $\frac{j \times 000 (9000 + j \times 000)}{(2000 + j \times 000) (2000)} = \frac{j \times (9 + j \times 1)}{(2 + j \times 1) (4 + j \times 1)}$ H(jw) = $=\frac{(2 \angle 90^{\circ}) \sqrt{9^{2}+2^{2}} / 12.521^{\circ}}{(\sqrt{2^{2}+2^{2}} / 45^{\circ})(\sqrt{4^{2}+2^{2}} / 26.565)}$ = 1.458 / (90+12.521°-45°-26.565°) = 1.458 L 30.956° ". Vo-standy stake = 8 x 1.456 cos (2000t + 30.956°) = 11.68 as (2000t + 30,956°) (1)





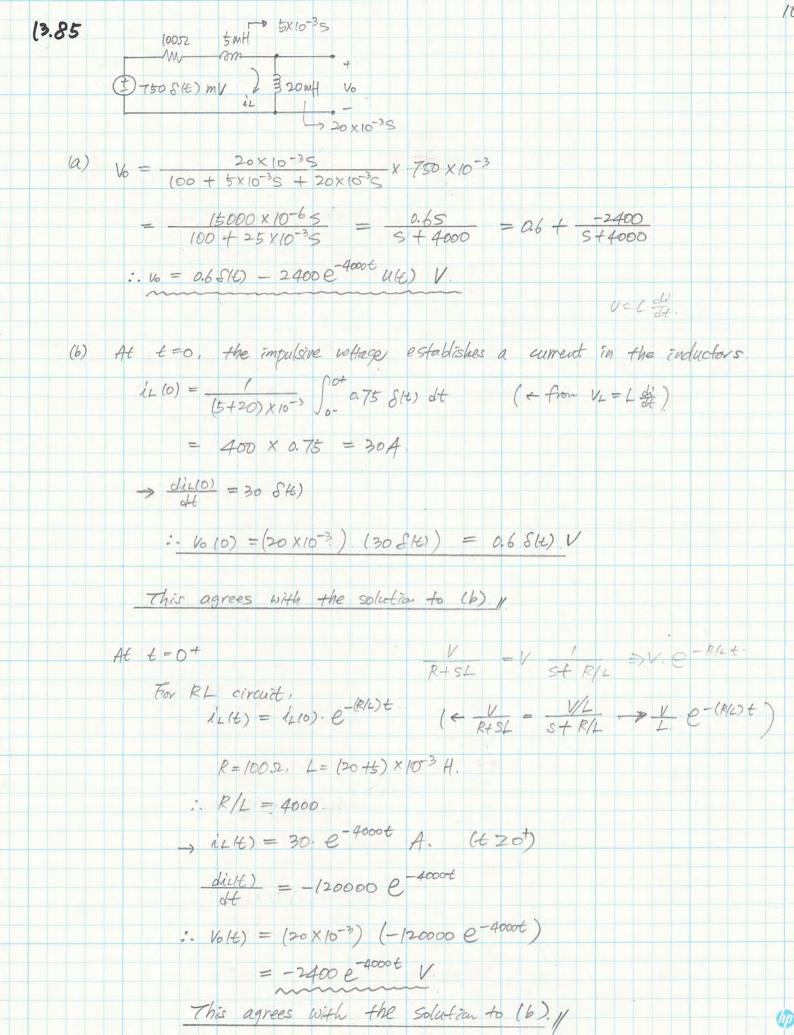




$$t_{1} = \frac{|625005 + 25 \times 10^{8}}{5450000} |_{S=0} = \frac{25 \times 10^{8}}{50000} = \frac{50000}{50000}$$

$$t_{2} = \frac{|625005 + 25 \times 10^{8}}{5} |_{S=-50000} = \frac{5025 \times 10^{8}}{50000} = \frac{112500}{50000}$$

$$\vdots |_{I_{0}} = \frac{|40511 + 2 \times 10^{8} + 4.5 \times 10^{8} + 2.5 \times 10^{8}}{50000} |_{I_{0}} |_{I_{0}}$$



14.5 $V_0 = \frac{y_{SC}y_{RL}}{R + y_{SC}y_{RL}} \quad V_{\lambda} \qquad \frac{y_{C}y_{RL}}{y_{C}} = \frac{R_L}{SC} = \frac{R_L}{1 + SR_LC}$ (a) | RL | RL | RL + R + SRRLC | RL + R + SR = S + /RC + /RC /H(jω)/ = /w² + (/κc + /κω)² (b) at w=0 -> /H(jw)/ is maximum. (c) :. / Hejas/max = YRC + VRLC = RL + R at w=wc > /H(jw) / = /H(jw) /max / 1/2 (d). /pc / /kc + /kc) = /kc + /kc /= : W= + (/RC + /RLC) = (/RC + /RLC).2 $W_c^2 = \left(\frac{1}{RC} + \frac{1}{RLC}\right)^2 = \left(\frac{R}{RRLC}\right)^2 = \left(\frac{1}{RC}\left(1 + \frac{R}{RL}\right)\right)^2$:. Wc = / (1+ RL) 20K2.

4nfi \$ 700kr Vo $W_{c} = \frac{1}{RC} \left(1 + \frac{R}{RL} \right)$ = 12500 (1 + 20/300) = 13.333 krad/sH(jo) = 300 = 0.9375

 $H(jac) = \frac{V_{RC}}{S + \frac{R + R_L}{RR_LC}} = \frac{13333.33}{13333.33}$ = 1.25 × 104 J (3333.333 + 13333.333 $= \frac{1.25 \times 10^4}{1.8856 \angle 45^\circ} = 0.6629 \angle -45^\circ$ $H(j0.2\omega_c) = \frac{1.25 \times 10^4}{j0.2 \times 13233.333 + 13333.333}$ $= \frac{1.25 \times 10^4}{13.579 \times 10^4 \times 11.31^\circ} = 0.9193 \times -11.31^\circ$ $H(j0.8wc) = \frac{1.25 \times 104}{5.25 \times 104}$ $= \frac{1.25 \times 10^{4}}{10.750 \times 10^{4} \angle \theta^{2} \cdot \theta^{75}} = 0.1163 \angle \theta^{2} \cdot \theta^{75}$ 14.13 Design a high-pass, RL passive filter Cutof frequency = 160 krad/s. L=25 mH. $V_{k} \circlearrowleft V_{k} \circlearrowleft V_{k} = \frac{1}{R} + \frac{1}{S} + \frac{1}{S} + \frac{1}{R} +$ WC = P/L :. R= WCL = 160 × 10° × 25 × 10-3 = 4600 = 4 / 52 (a) with RL (6) SLR + RRL + SLRL = S(LR + LRL) + RRL :. RRL = 150 × 103 $R_{L} = \frac{150 \times 10^{3} \times 100}{2500}$ RRL = 150 × 103 (LR + LRL) = 60 Ks RL (R-150×103L) = 150×103LR -