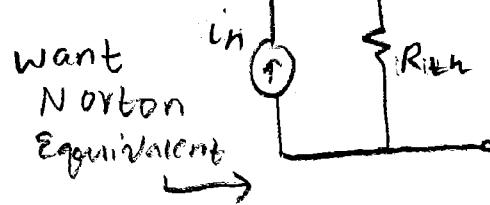
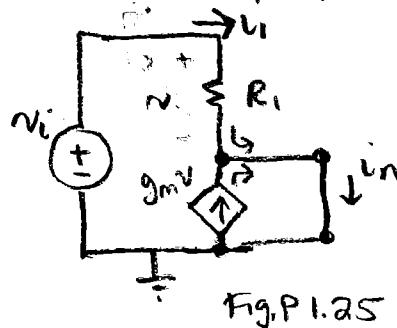


# EE 331 Spring 2014 Homework #0 solutions

1.24)

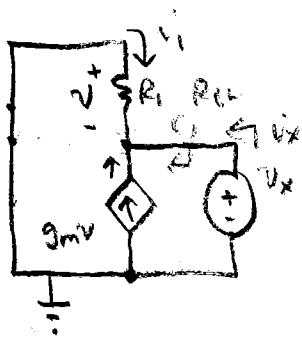


Kinda Like Example 1.2, do lots of KCL/KVL :

$$i_n = i_1 + g_m v \quad , \quad i_1 = G_v v_i$$

$$i_n = v_i(G_v + g_m) = \left(\frac{1}{10k} + 0.002\right) v_i = 0.0021 v_i$$

Rth:



$$R_{th} = \frac{v_x}{i_x}$$

KCL again:

$$-i_1 - g_m v_i - i_x = 0$$

$$i_x = -\left(\frac{v}{R_1}\right) - g_m(-v_x) \quad \left\{ \begin{matrix} v_x = -v \\ i_x = v_x \left(\frac{1}{R_1} + g_m\right) \end{matrix} \right.$$

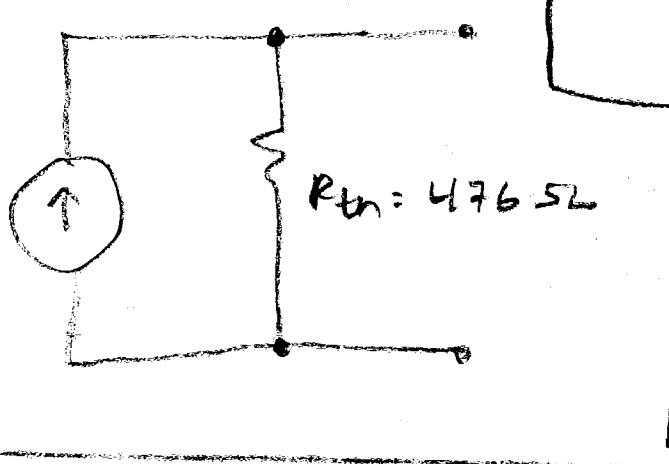
$$\therefore \frac{v_x}{i_x} = R_{th} = \frac{1}{\left(\frac{1}{R_1} + g_m\right)} = \frac{1}{\left(\frac{1}{10k} + 0.002\right)}$$

∴ Solution

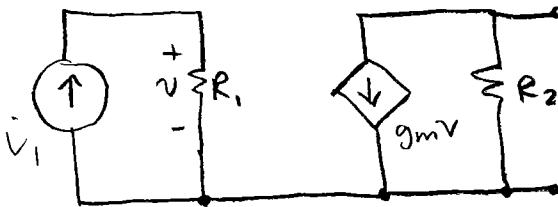
$$\approx 476 \Omega$$

$$v_n = (2.1 \times 10^{-3}) v_s$$

$$R_{th} = 476.5 \Omega$$



1.29)



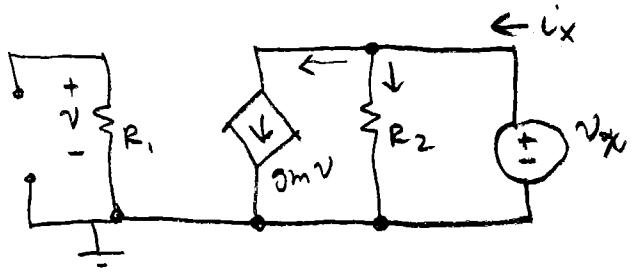
$$g_m = 0.0025 \text{ S}$$

$$R_1 = 200 \text{ k}\Omega$$

$$R_2 = 1.5 \text{ M}\Omega$$

Find  $R_{th}$ :

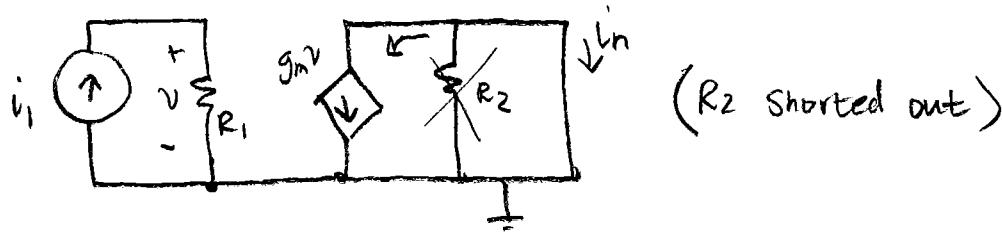
$$R_{th} = \frac{v_x}{i_x}$$



$$\text{KCL at } v_x: -i_x + \frac{v_x}{R_2} + g_m v \xrightarrow{v=0} 0$$

$$\therefore \frac{v_x}{i_x} = R_{th} = R_2 = 1.5 \text{ M}\Omega$$

short output to find  $i_n$ :



$$\text{KCL: } i_n = -g_m v \quad v = i_i R_1$$

$$i_n = -g_m R_1 i_i$$

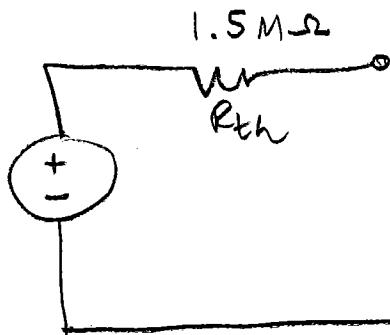
$$\begin{aligned} \therefore v_{th} &= i_n R_{th} = (-g_m R_1 i_i) (R_{th}) \\ &= -(0.0025)(1.5 \text{ M}) \xrightarrow{v_{th} \text{ in } \text{V}_s} v_s \\ &= -3750 \text{ V}_s \end{aligned}$$

Solution

$$v_{th} =$$

$$-3750 \text{ V}_s$$

$$v_1$$



problem 1b2 were have wrong #s  
but use other methods to solve FYI

Ee331, spring 2012

Solution to HWO

**Problem 1**

$$i = -g_m(i_1 R_1) \Rightarrow i_1 = 0, V_{\infty} = v_i$$

$$R_h = \frac{V}{I_{\infty}} = \frac{V}{(1+g_m R_1)v_i / R_1} = \frac{R_1}{1+g_m R_1}$$

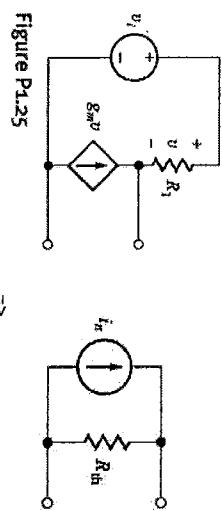
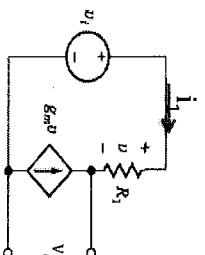
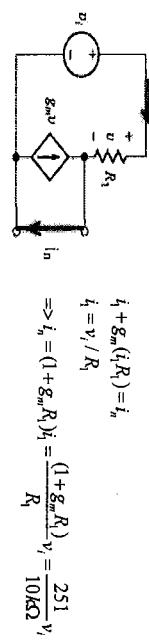


Figure P1.25

$i_n$  represents the current when output circuit is short



$$i_1 + g_m(i_1 R_1) = i_n$$

$$i_1 = v_i / R_1$$

$$\Rightarrow i_n = (1 + g_m R_1) i_1 = \frac{(1 + g_m R_1) v_i}{R_1} = \frac{251}{10 k\Omega} v_i$$

$R_h$  represents the equivalent resistance present at the output terminals with all independent sources set at zero.

There are three methods to solve  $R_h$ .

Method 1: open circuit voltage divided by short circuit current

$$R_h = \frac{V}{I_s}$$

$I_s$  is the output current when output circuit is short, same with  $i_n$ ,  
 $V_s$  is the output voltage when output circuit is open.

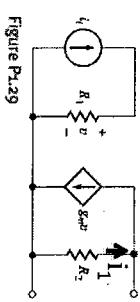
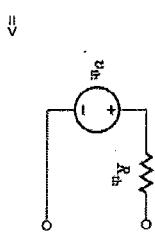
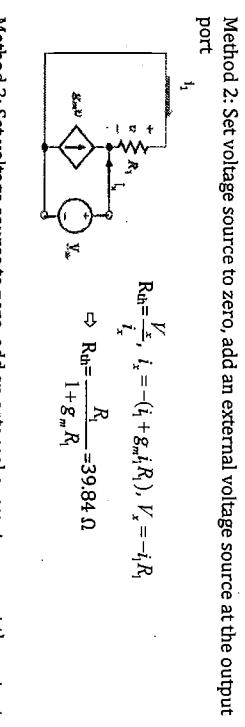


Figure P1.29



$\Rightarrow$



Method 2: Set voltage source to zero, add an external voltage source at the output port

$$R_h = \frac{V_x}{i_x}, i_x = -(i_1 + g_m i_1 R_1), V_x = -i_1 R_1$$

$$\Leftrightarrow R_h = \frac{R_1}{1 + g_m R_1} = 39.84 \Omega$$

Method 3: Set voltage source to zero, add an external current source at the output port

$$i_x = -(i_1 + g_m i_1 R_1), V_x = -i_1 R_1$$

$$R_h = \frac{V_x}{i_x} = \frac{-i_1 R_1}{-(i_1 + g_m i_1 R_1)} = \frac{R_1}{1 + g_m R_1} = 39.84 \Omega$$

**Problem 2:**

$V_{th}$  represents the equivalent voltage when output is open.

$$v = i_1 R_1$$

$$i_1 = g_m v = i_1 R_1$$

$$V_{th} = i_1 R_2 = R_1 R_2 g_m i_1$$

$R_{th}$  represents the equivalent resistance when all independent sources are zero.

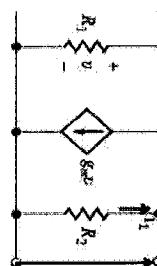
Three ways to solve  $R_{th}$

Method 1: open circuit voltage divided by short circuit current

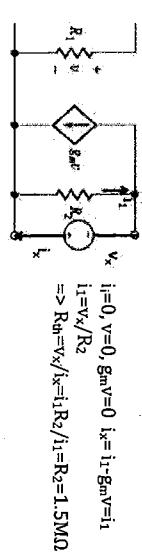
$$R_{th} = \frac{V_{oc}}{I_{sc}}$$

$$V_{oc} = V_{in} = R_1 R_2 g_m i_1$$

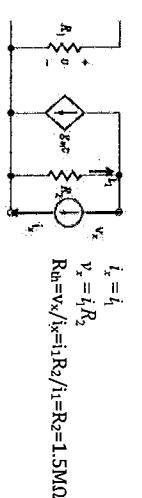
$$I_{sc} = R_1 R_2 g_m i_1$$



Method 2: Set current source to zero, add an external voltage source at output



Method 3: set current source to zero, add an external current source at output



### Problem 3

Expressions for  $V_1$ ,  $I_2$  and  $I_3$  are given by:

$$V_1 = \frac{V}{1 + \left( \frac{1}{R_3} + \frac{1}{R_2} \right) \frac{1}{R_1}}$$

$$I_2 = \frac{V - V_1}{R_2}$$

$$I_3 = \frac{V - V_1}{R_3}$$

Nominal values are:

$$V_1^{nom} = \frac{1}{1 + \left( \frac{1}{1k} + \frac{1}{30k} \right) \frac{1}{24k}} \approx 0.75V$$

$$I_2^{nom} = \frac{1 - 0.7489}{30k} \approx 8.37\mu A$$

$$I_3^{nom} = \frac{1 - 0.7489}{11k} \approx 22.83\mu A$$

According to the expression of  $V_1$ , the max and minimum values of  $V_1$  are:

$$V_1^{\max} = \frac{1 \times 1.05}{1 + \frac{1}{11k \times 0.9} + \frac{1}{30k \times 0.9}} \approx 0.82V$$

$$V_1^{\min} = \frac{1 \times 0.95}{1 + \frac{1}{11k \times 1.1} + \frac{1}{30k \times 1.1}} \approx 0.67V$$

Worst-case values of  $I_2$  and  $I_3$  are:

$$I_2^{\max} = \frac{V - V_1^{\min}}{R_2^{\max}} = \frac{1 - 0.67}{30k \times 0.9} = 12.22\mu A$$

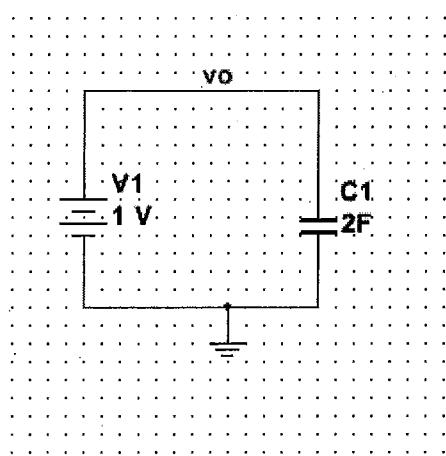
$$I_2^{\min} = \frac{V - V_1^{\max}}{R_2^{\min}} = \frac{1 - 0.82}{10k \times 1.1} = 5.45\mu A$$

$$I_3^{\max} = \frac{V - V_1^{\min}}{R_3^{\max}} = \frac{1 - 0.67}{11k \times 0.9} = 33.33\mu A$$

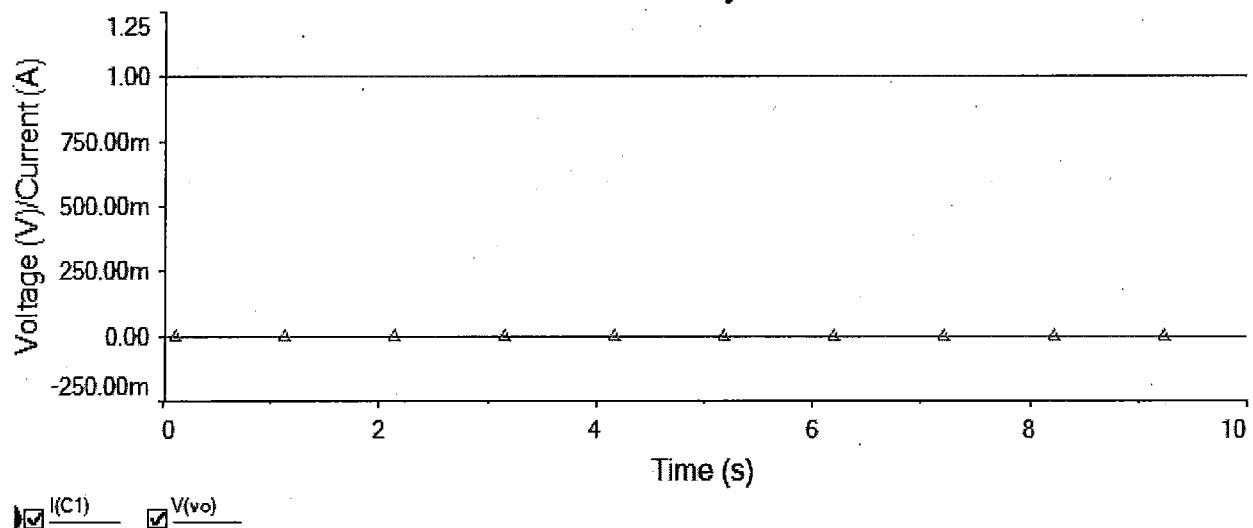
$$I_3^{\min} = \frac{V - V_1^{\max}}{R_3^{\min}} = \frac{1 - 0.82}{11k \times 1.1} = 14.88\mu A$$

### Problem 4 Solution

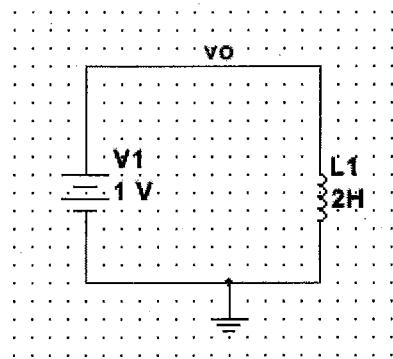
a) and b)



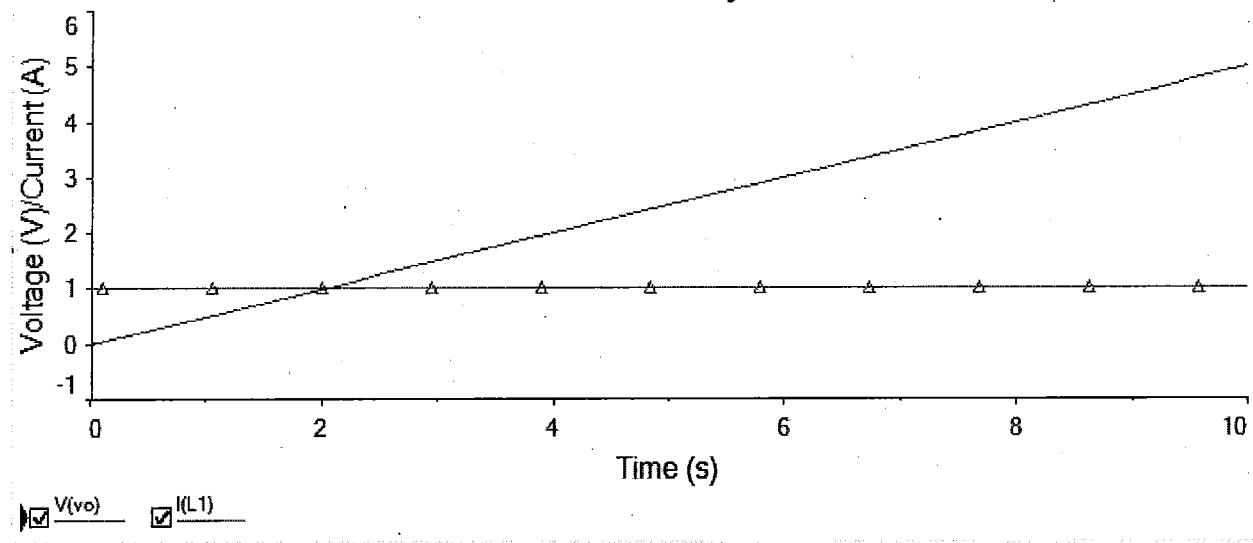
4ab  
Transient Analysis



C) and d)



4cd  
Transient Analysis



## Problem 5

- a) The first step in finding the transfer function is to construct the s-domain equivalent circuit. By definition, the transfer function is the ratio of  $\frac{V_o}{V_0}$ , which can be computed from a single node-voltage equation. Summing the currents away from the upper node generates

$$\frac{V_o - V_0}{1000} + \frac{V_o}{250 + 0.05s} + \frac{V_o s}{10^6} = 0$$

Solve  $V_o$ ,

$$V_o = \frac{1000(s + 5000)V_0}{s^2 + 6000s + 25 \times 10^6}$$

Hence the transfer function is

$$H(s) = \frac{V_o}{V_0} = \frac{1000(s + 5000)}{s^2 + 6000s + 25 \times 10^6}$$

The poles of  $H(s)$  are the roots of the denominator polynomial. Therefore

$$\begin{aligned} -p_1 &= -3000 - j4000 \\ -p_2 &= -3000 + j4000 \end{aligned}$$

The zeros of  $H(s)$  are the roots of the numerator polynomial; thus

$$-z_1 = -5000$$

For the impulse response, let

$$\begin{aligned} V_o &= \frac{1000(s + 5000)}{s^2 + 6000s + 25 \times 10^6} = \frac{K_1}{s + 3000 - j4000} + \frac{K_1^*}{s + 3000 + j4000} \\ K_1 &= 500 - j250 = 559.017 \angle -26.57^\circ \\ K_1^* &= 500 + j250 = 559.017 \angle 26.57^\circ \end{aligned}$$

Test the solutions with the zero of  $H(s)$

$$H(-5000) = \frac{500 - j250}{-5000 + 3000 - j4000} + \frac{500 + j250}{-5000 + 3000 + j4000} = 0$$

Then, transform back to time domain,

$$y(t) = h(t) = 1118e^{-3000t} \cos(4000t - 26.57^\circ)u(t)$$

For the response of the input source, let

$$V_{oAC} = \frac{1000(s + 5000)V_0}{s^2 + 6000s + 25 \times 10^6}$$

$$V_o = \frac{15000(s + 5000)}{s(s^2 + 6000s + 25 \times 10^6)} = \frac{K_2}{s} + \frac{K_3}{s + 3000 - j4000} + \frac{K_3^*}{s + 3000 + j4000}$$

$$\begin{aligned} K_2 &= 3 \\ K_3 &= -1.5 - j0.75 = 1.6771 \angle -153.44^\circ \\ K_3^* &= -1.5 + j0.75 = 1.6771 \angle 153.44^\circ \end{aligned}$$

Test the root of zero

$$\frac{3}{-5000} + \frac{-1.5 - j0.75}{-5000 + 3000 - j4000} + \frac{-1.5 + j0.75}{-5000 + 3000 + j4000} = 0$$

Then the response due to the input is

$$y(t) = [3 + 3.35e^{-3000t} \cos(4000t - 153.44^\circ)]u(t)$$

We can see the response includes a DC which is 3 V and a fast decaying cosine wave.

- b) Multisim simulation result is shown below:

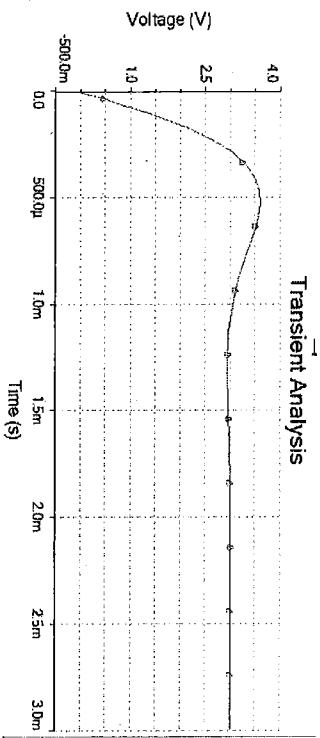


Figure 1 Transient response to  $v_{AC}$

The steady state voltage is 3V, consistent with solution in part a).

## Problem 6

Applying superposition,  $V_o = V_{oDC} + V_{oAC}$ .  $V_{oDC}$  is the response of the DC source  $v_{DC}$ , and  $V_{oAC}$  is the response of the AC source  $v_{AC}$ . Then in s-domain, we have

$$V_o = \frac{1000(s + 5000)(V_0 + V_1)}{s^2 + 6000s + 25 \times 10^6} = V_{oAC} + V_{oDC}$$

We have got  $V_{oAC}$  in the last problem and

The frequency of the voltage source is  $10^6$  rad/s, hence we evaluate  $H(s)$  at  $H(j10^6)$ :

$$H(j10^6) = \frac{1000(j10^6 + 5000)}{(j10^6)^2 + 6000(j10^6) + 25 \times 10^6} \approx 0.0012 - 90^\circ$$

Then

$$v_{oac} = 0.005\cos(10^6t - 60^\circ)u(t)$$

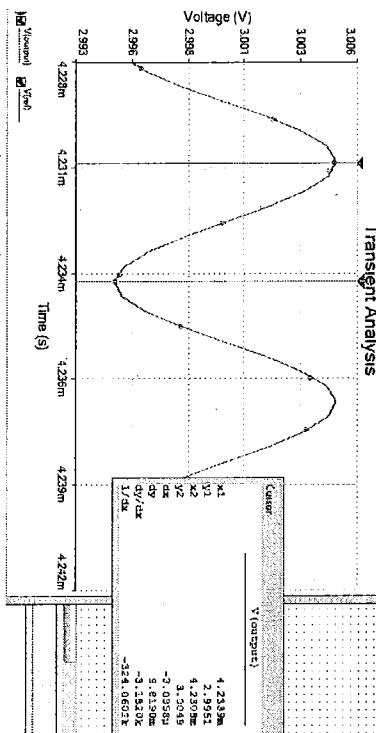
Then

$$\begin{aligned} v_o &= v_{oac} + v_{vac} \\ &= [3 + 0.005\cos(10^6t - 60^\circ) \\ &\quad + 1.6771e^{-3000t}\cos(4000t - 153.44^\circ)]u(t) \end{aligned}$$

The steady-state response is let time goes to infinity, thus the fast decaying cosine wave can be ignored, then

$$v_{o,steady} = [3 + 0.005\cos(10^6t - 60^\circ)]u(t)$$

b) Steady state output simulated by Multisim is shown below:

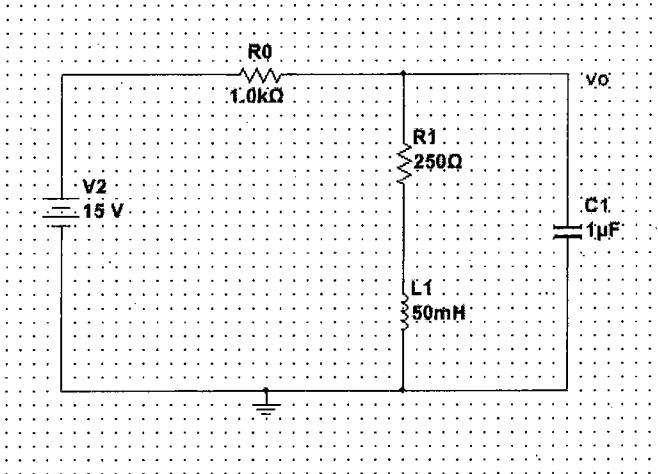


To verify the phase value, the steady output waveform in red is compared with a reference waveform of  $3+0.005\cos(10^6t-60^\circ)$  in green. As can be seen, they are completely overlapped in steady state.

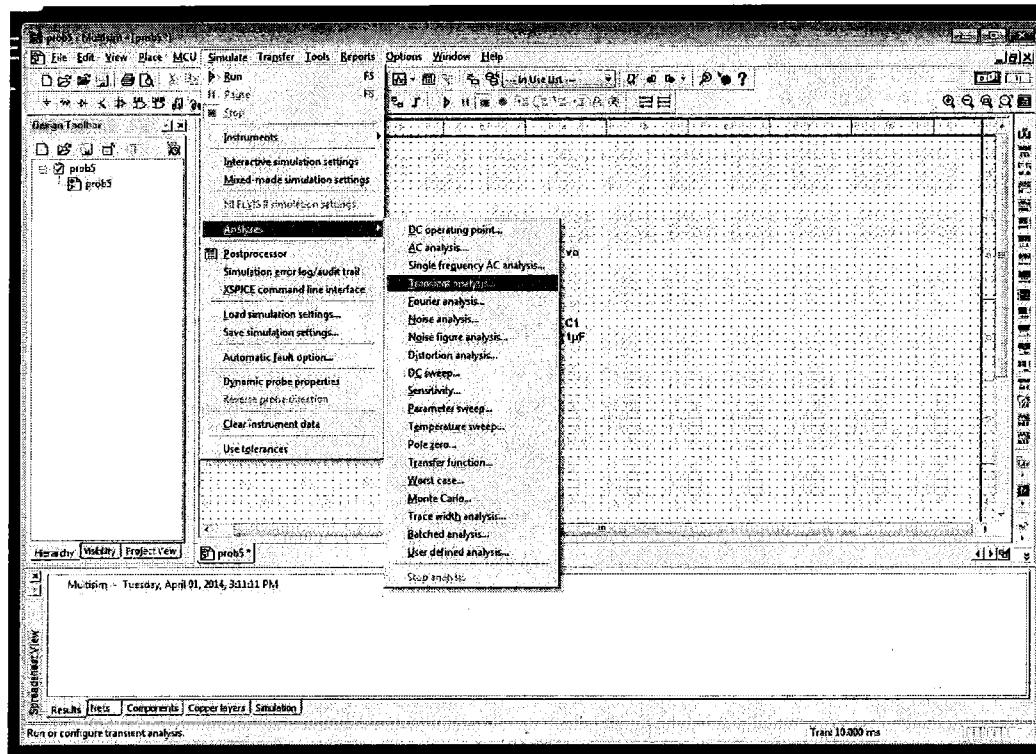
## Homework #0

### Problem 5. b) solution

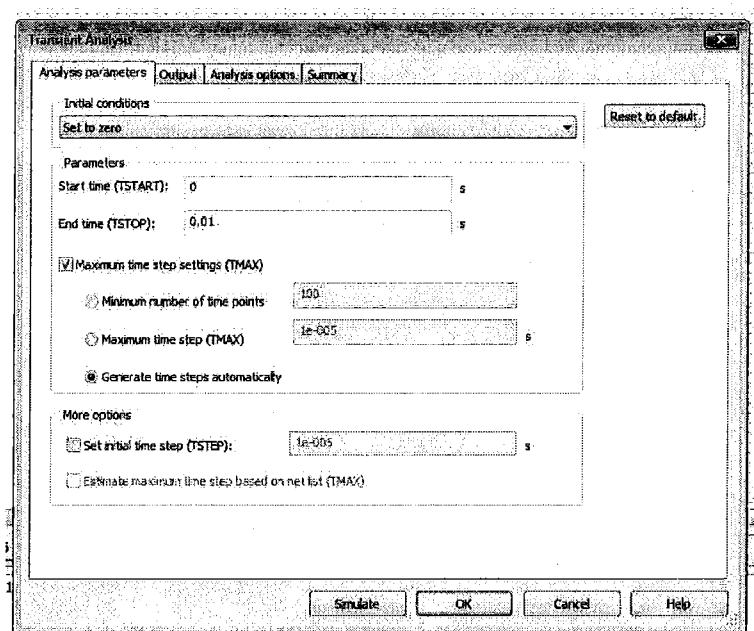
Using Multisim, put together the following circuit. I labeled the node  $v_O$  for convenience:



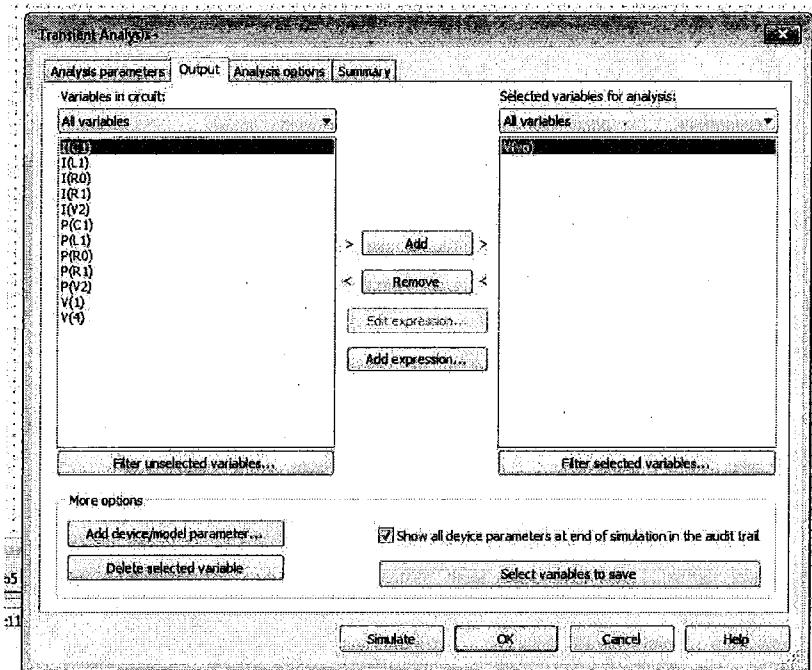
Next, run a Transient Analysis:



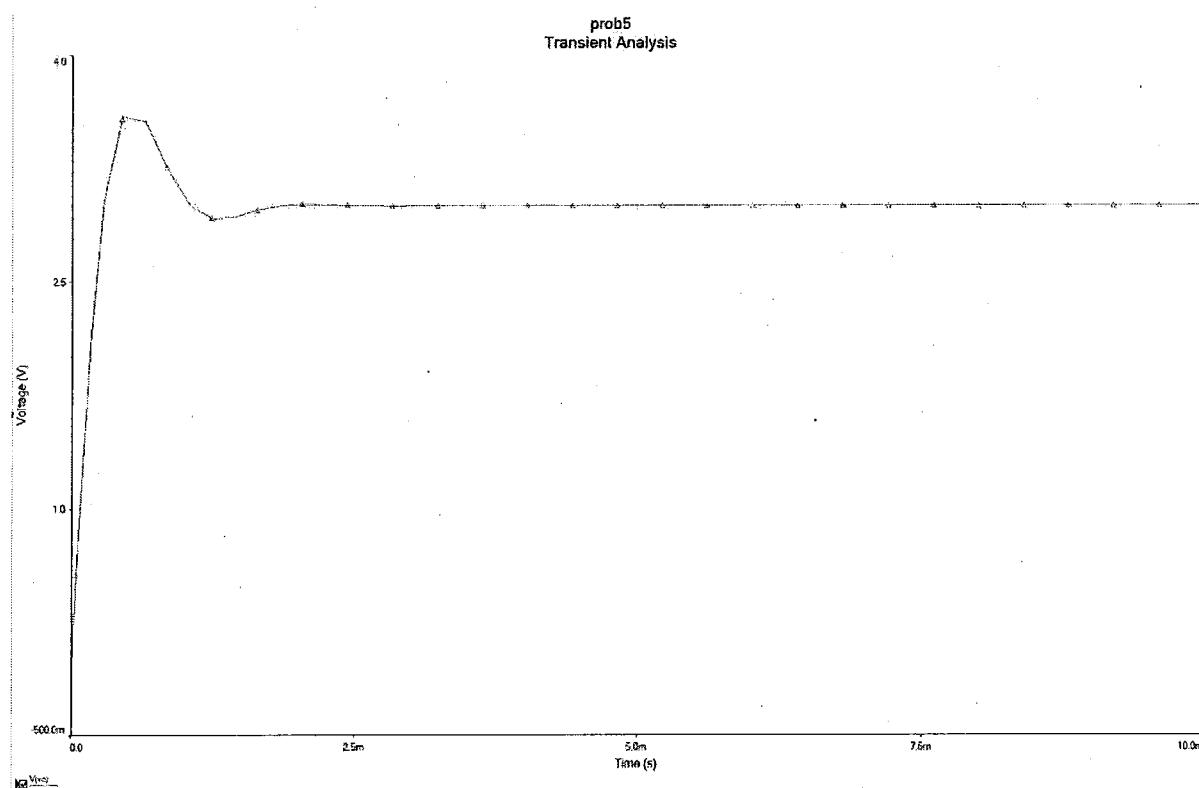
I set the stop time (TSTOP) to 10 mS, but you can pick whatever amount of time makes a good-looking plot. I kept everything else set to default:



Next, I went to the Output tab and selected V(vo) so the graph will display the output voltage we want for this problem:



Last, hit the "Simulate" button at the bottom of the Transient Analysis dialog, and a graph like this should appear showing the Transient Response at the node vo:



## Homework #0

### Problem 6. b) solution

Solution is similar to Problem 5. b), but notice that the sinusoidal voltage input for Multisim requires RMS voltage =  $V_{\text{amplitude}}/1.41 = 5/1.41 = 3.54 \text{ V}$ , and  $10^6 \text{ rad/sec}$  frequency is converted to kHz.

