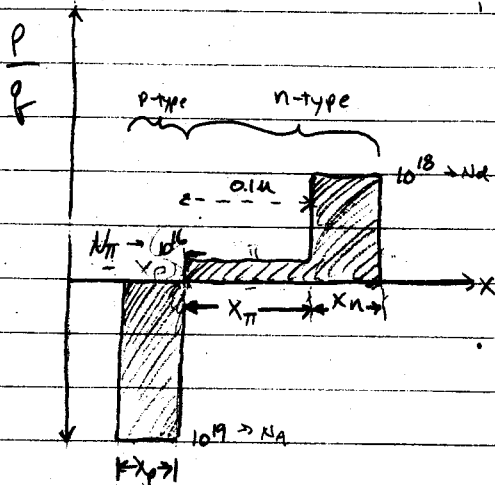


1. (a)

Silicon: $\epsilon_0 k = 11.7 (8.85 \times 10^{-14})$

$$N_A \sim 10^{19} \text{ cm}^{-3} \quad N_T \sim 10^{16} \text{ cm}^{-3} \quad N_D \sim 10^{18} \text{ cm}^{-3}$$



$$\text{Charge Neutrality } x_p N_A = x_n N_D$$

$$E_1 = -\frac{q N_A x_p}{\epsilon_0}$$

$$E_2 = -\frac{q N_D x_n}{\epsilon_0} = -E_1 + \frac{q N_T x_n}{\epsilon_0}$$

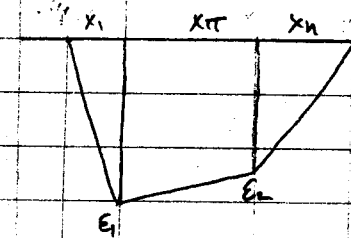
$$\phi_i = \frac{kT}{q} \ln \left(\frac{N_A N_D}{n_i^2} \right) = 0.026 \ln \left(\frac{10^{19} 10^{18}}{(1.5 \times 10^{10})^2} \right) = 0.9967 \text{ V}$$

$$\phi_i = \frac{x_p (-E_1)}{2} + \frac{x_n (-E_2 - E_1)}{2} + \frac{x_n (-E_2)}{2}$$

$$= \frac{x_p^2 \frac{q N_A}{2 \epsilon_0}}{2} + \frac{x_n x_p N_D}{2 \epsilon_0} + \frac{x_n x_p N_A}{2 \epsilon_0} + \frac{x_n^2 \frac{q N_D}{2 \epsilon_0}}{2}$$

 ϵ

$$\frac{2k\epsilon_0\phi}{q} = \left[x_p^2 N_A + x_n x_p N_D + x_n x_p N_A + x_n^2 N_D \right]$$

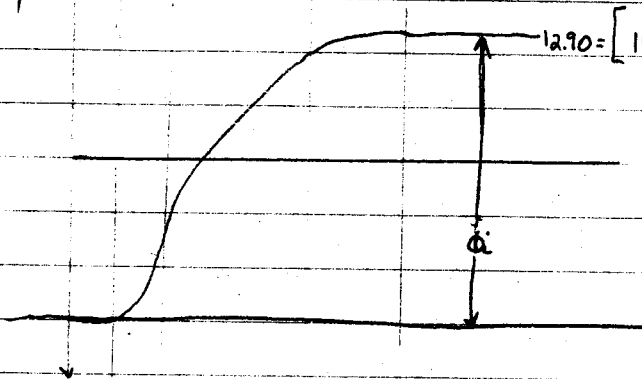


$$\frac{2k\epsilon_0\phi}{q} = \left[\frac{(x_n N_T + x_n N_D)^2}{N_A} + x_n x_p N_D + x_n (x_n N_T + x_n N_D) + x_n^2 N_D \right]$$

$$\frac{2k\epsilon_0\phi}{q} = \left[\frac{x_n^2 N_T^2}{N_A} + \frac{2x_n N_T x_n N_D}{N_A} + \frac{x_n^2 N_D^2}{N_A} + x_n x_p N_D + x_n^2 N_T + x_n x_p N_D + x_n^2 N_D \right]$$

$$\frac{2k\epsilon_0\phi}{q N_T x_n^2} = \left[\frac{x_n^2 N_T^2}{N_A N_T x_n^2} + \frac{2x_n N_T x_n N_D}{N_A N_T x_n^2} + \frac{x_n^2 N_D^2}{N_A N_T x_n^2} + \frac{x_n x_p N_D}{N_T x_n^2} + \frac{x_n^2 N_T}{x_n^2 N_T} + \frac{x_n x_p N_D}{x_n^2 N_T} + \frac{x_n^2 N_D}{x_n^2 N_T} \right]$$

$$12.90 = \left[\frac{N_T}{N_A} + \frac{2N_D}{N_A} \left(\frac{x_n}{x_p} \right) + \frac{N_D^2}{N_A N_T} \left(\frac{x_n}{x_p} \right)^2 + \frac{N_D}{N_T} \left(\frac{x_n}{x_p} \right) + 1 + \frac{N_D}{N_T} \left(\frac{x_n}{x_p} \right) + \frac{N_D}{N_T} \left(\frac{x_n}{x_p} \right)^2 \right]$$

 ϕ 

$$12.90 = \left[110 \left(\frac{x_n}{x_p} \right)^2 + 200.2 \left(\frac{x_n}{x_p} \right) + 1.001 \right] \quad \frac{x_n}{x_p} = 0.05761$$

$$x_n = 5.761 \times 10^{-3} \text{ cm}$$

$$x_p = \frac{(0.1 \times 10^{-3}) (10^{16}) + (5.761 \times 10^{-3}) (10^{18})}{10^{19}} = 6.761 \times 10^{-8} \text{ cm}$$

1.B) $E_{\max}$ OF PIN DIODE:

$$E_1 = -\frac{q N_A x_p}{\epsilon_0} = -\frac{(1.6 \times 10^{-19})(10^4)(6.361 \times 10^{-8})}{(11.7)(8.85 \times 10^{-14})} = -1.015 \times 10^5 \frac{V}{cm}$$

$$E_2 = -\frac{q N_A x_n}{\epsilon_0} = -\frac{(1.6 \times 10^{-19})(10^8)(5.76 \times 10^{-7})}{(11.7)(8.85 \times 10^{-14})} = -8.90 \times 10^4 \frac{V}{cm}$$

$E_{\max}$ OF PN DIODE WITHOUT INTRINSIC REGION

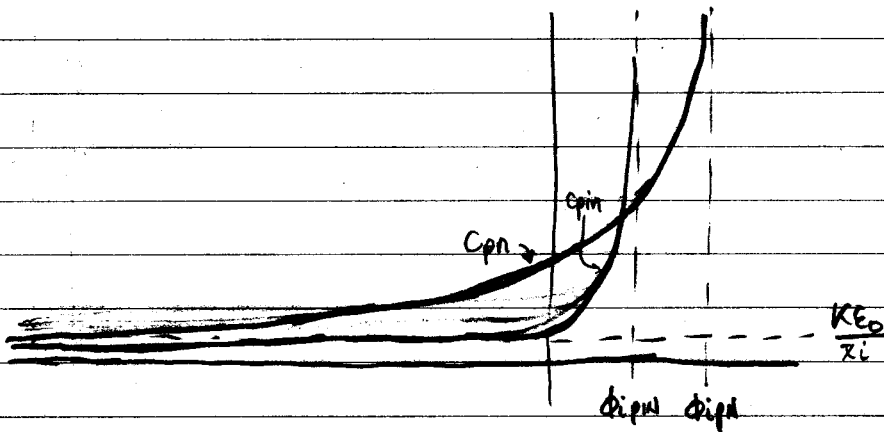
$$E_{\max} = -\left[\frac{2q\phi_i N_A N_D}{\epsilon_0 (N_A + N_D)}\right]^{\frac{1}{2}} = -\left[\frac{2(1.6 \times 10^{-19})(0.9467)(10^4)(10^8)}{(11.7)(8.85 \times 10^{-14})(10^4 + 10^8)}\right]^{\frac{1}{2}} = -5.292 \times 10^5 \frac{V}{cm}$$

$E_{\max}$ WITHOUT INTRINSIC REGION IS ABOUT 5 TIMES LARGER BECAUSE THE INTRINSIC REGION INCREASES THE AMOUNT OF VOLTAGE DROPPED THROUGH THE DEVICE.

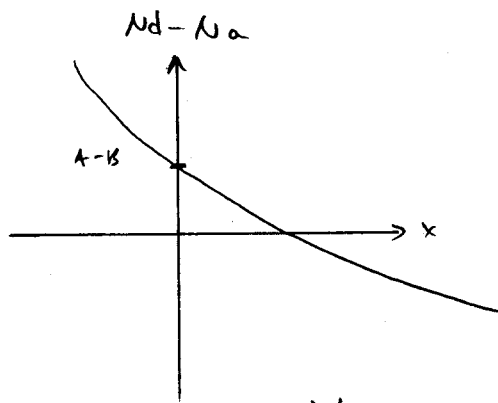
1.C) AS LONG AS INTRINSIC REGION IS FULLY DEPLETED, $x_p, x_n \ll x_i$ AND $x_d \approx x_i$

$$\text{SO } C = \frac{\epsilon_0}{x_i}$$

↳ FORWARD BIAS $\rightarrow$ LIGHTER DOPED N REGION NO LONGER FULLY DEPLETED, SO $N_A = 10^{17}, N_D = 10^{18}$



2a)

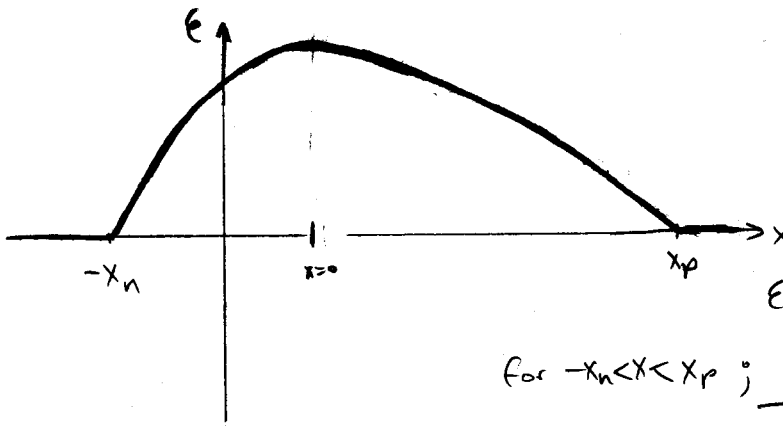
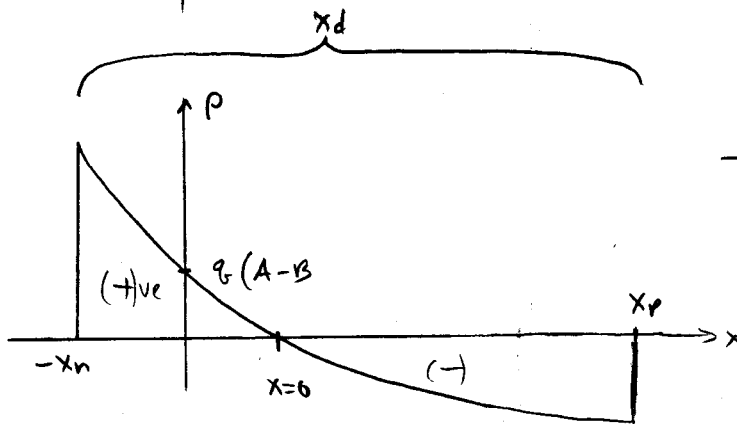


$$N_d - N_a = A e^{-\frac{x}{L}} - B$$

$$\rho(x) = q (N_d - N_a)$$

$$\rho(x) = q (A e^{-\frac{x}{L}} - B)$$

$$\text{for } -x_n < x < x_p$$



$$E(x) = \int_{-\infty}^x \frac{\rho(x) dx}{k \epsilon_0} = \frac{q}{k \epsilon_0} \int_{-x_n}^x \rho(x) dx$$

$$= \frac{q}{k \epsilon_0} \int_{-x_n}^x (A e^{-\frac{x}{L}} - B) dx$$

$$= \frac{q}{k \epsilon_0} \left[-L A e^{-\frac{x}{L}} - B x \right] \Big|_{-x_n}^x$$

$$= -\frac{q}{k \epsilon_0} \left[B x_n - L A e^{\frac{x_n}{L}} + L A e^{-\frac{x}{L}} + B x \right]$$

const; C_1

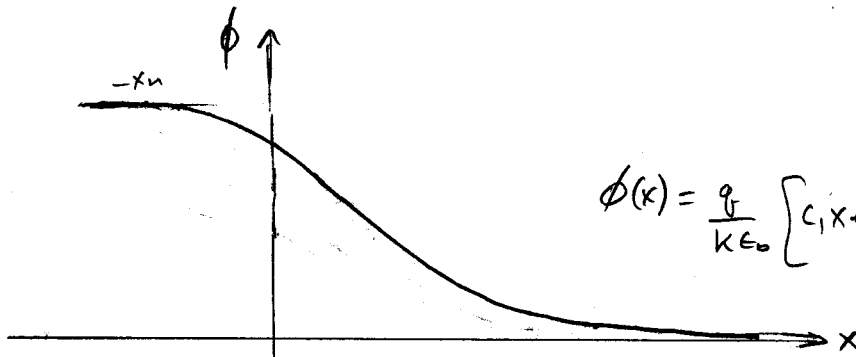
$$E(x) = \frac{-q}{k \epsilon_0} \left[C_1 + L A e^{-\frac{x}{L}} + B x \right]$$

$$\text{for } -x_n < x < x_p; \quad E(x) = 0 \quad \text{else}$$

$$\phi(x) = - \int_{-\infty}^x E(x) dx = \int_{-x_n}^x E(x) dx$$

$$= -\frac{q}{k \epsilon_0} \left[C_1 x + \frac{1}{2} B x^2 - L^2 A e^{-\frac{x}{L}} \right] \Big|_{-x_n}^x$$

$$\phi(x) = \frac{q}{k \epsilon_0} \left[C_1 x + \frac{1}{2} B x^2 - L^2 A e^{-\frac{x}{L}} - C_2 \right]$$



$$\text{where } C_2 = C_1 x_n + \frac{1}{2} B x_n^2 - L^2 A e^{\frac{x_n}{L}}$$

2b)

$$\phi_i = \frac{kT}{q} \ln \frac{N_a N_d}{n_i^2} = \frac{kT}{q} \ln \left[\frac{(B - A e^{-x_p/L})(A e^{x_n/L} - B)}{n_i^2} \right]$$

and previously

$$(*) \phi_i = \frac{q}{\kappa \epsilon_0} \left(L^2 A e^{-\frac{x}{L}} + \frac{1}{2} B x^2 + C_1 x - C_2 \right)$$

To determine x_n & x_p use to find $x_d = x_n + x_p$ use:

$$\int_{-x_n}^{x_p} \rho(x) dx = 0$$

$$\text{eq (1): } L A e^{-\frac{x_p}{L}} + B x_p - L A e^{\frac{x_n}{L}} + B x_n = 0$$

and also

$$\text{eq (2): } \phi_i = - \int_{-x_n}^{x_p} E(x) dx = \frac{q}{\kappa \epsilon_0} \left(C_1 x_p + \frac{1}{2} B x_p^2 - L^2 A e^{-\frac{x_n}{L}} \right)$$

(because x_n term cancelled the C_2 term)

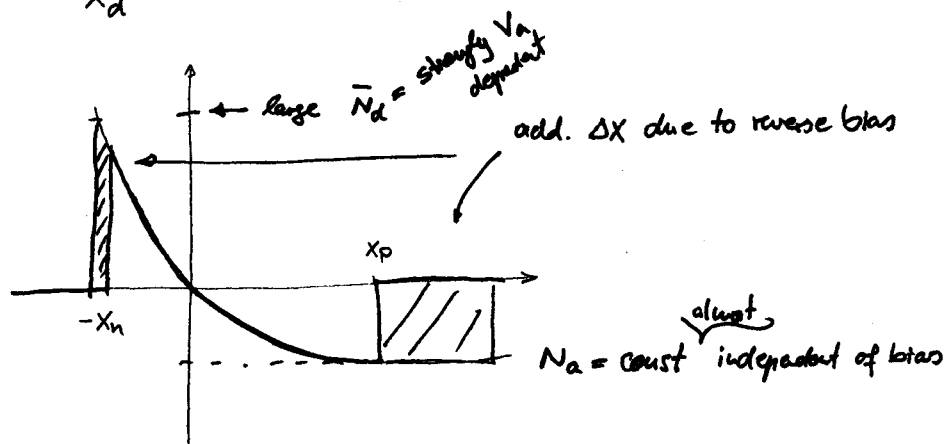
Solve eq (1) and (2) for two unknowns x_n & x_p

and ϕ_i can be solved using eq (*)

2)

c) capacitance variation with applied large reverse bias ($|V_a| \gg \phi_i$)

$$C' = \frac{k\epsilon_0}{x_d} \quad (\text{see lecture notes})$$



$$\Delta x_n \cdot \bar{N}_d = \Delta x_p \cdot N_a \quad (\text{charge neutrality})$$

$$\Delta x_n = \underbrace{\frac{N_a}{\bar{N}_d}}_{\substack{\text{really small number is} \\ \text{limit}}} \cdot \Delta x_p$$

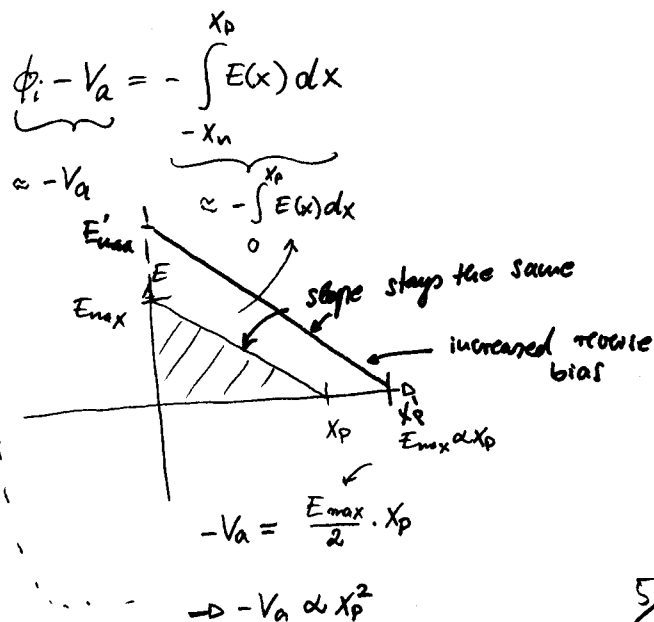
$$\Rightarrow x_d = \underbrace{x_n + \Delta x_n}_{\text{small}} + x_p + \Delta x_p \cong x_p$$

$$\Rightarrow C' = \frac{k\epsilon_0}{x_p}$$

Now need to find $x_p(V_a)$

$$\frac{1}{x_p} \propto (-V_a)^{-1/2}$$

$$\Rightarrow C' \propto \frac{1}{\sqrt{|V_a|}}$$



3)

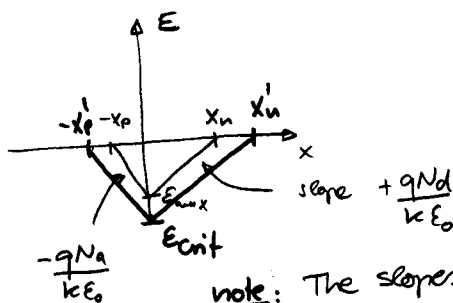
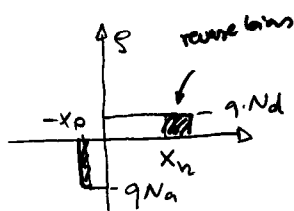
Calculate breakdown voltage at $T = 300\text{K}$ of an abrupt silicon diode

a) $N_d = 10^{19} \text{ cm}^{-3}$ $W_n = 200 \mu\text{m}$
 $N_a = 10^{16} \text{ cm}^{-3}$ $W_p = 0.5 \mu\text{m}$

i) Avalanche breakdown

$\Rightarrow$ need to take E_{crit} of lighter doped region since most of high field region is on that side (controls slope of E and scattering lifetime)

Plot lecture notes: $E_{\text{crit}} (10^{16} \text{ cm}^{-3}) = 4 \cdot 10^5 \text{ V/cm}$



note: The slopes don't change.
 $\Rightarrow$ if you know $E_{\text{crit}} \Rightarrow x_n', x_p'$

x_p' : $E(x) = E_{\text{crit}} - \frac{qN_a}{kE_0} x$

x_n' : $E(x) = E_{\text{crit}} + \frac{qN_d}{kE_0} x$

also: $E(x_n') = 0 \Rightarrow x_n' = -\frac{E_{\text{crit}} k E_0}{q N_d} = \frac{|E_{\text{crit}}| k E_0}{q N_d}$
 $E(-x_p') = 0 \Rightarrow x_p' = -\frac{E_{\text{crit}} k E_0}{q N_a} = \frac{|E_{\text{crit}}| k E_0}{q N_a}$

plug-in numbers: $x_n' = 2.58 \cdot 10^{-7} \text{ cm} = 2.58 \mu\text{m}$

$x_p' = 2.58 \cdot 10^{-4} \text{ cm} = 2.58 \mu\text{m}$

$\phi_i - V_a = - \int_{-x_p'}^{x_n'} E(x) dx = \frac{1}{2} E_{\text{crit}} (x_n' + x_p') = 51.65 \text{ V}$
 $\Rightarrow -V_a = 50.752 \text{ eV}$

$\phi_i = \frac{kT}{q} \ln \left(\frac{N_a N_d}{n_i^2} \right) = 0.898 \text{ V}$

3)

a)

ii) Zener breakdown

Doesn't happen at $N_a = 10^{16} \text{ cm}^{-3} \Rightarrow$ both doping concentrations need to be at least $\approx 10^{18} \text{ cm}^{-3}$ (see plot)

Basically X_d is too large if you have lightly doped region.

iii) Punch-through breakdown

$$X_n' = 2.58 \text{ nm} \ll W_n = 200 \mu\text{m}$$

$$X_p' = 2.58 \mu\text{m} > W_p = 0.5 \mu\text{m}$$

$\Rightarrow$ breakdown will happen via punch-through

$$X_p' = 0.5 \mu\text{m} \rightarrow \phi_i - V_a$$

$$X_p' = \left(\frac{2k\epsilon_0}{q} (\phi_i - V_a) \frac{N_d}{N_a(N_a + N_d)} \right)^{1/2}$$

$$\Rightarrow X_p'^2 \cdot \frac{N_a(N_a + N_d)}{N_d} \cdot \frac{q}{2k\epsilon_0} = \phi_i - V_a$$

$$-V_a = X_p'^2 \cdot \frac{N_a(N_a + N_d)}{N_d} \cdot \frac{q}{2k\epsilon_0} - \phi_i$$

$$-V_a = 1.935 - 0.898 \text{ V} = 1.037 \text{ V}$$

breakdown voltage is: $-V_a = 1.037 \text{ V}$

3)

b) $N_d = 10^{19} \text{ cm}^{-3}$ $W_n = 200 \mu\text{m}$
 $N_a = 10^{18} \text{ cm}^{-3}$ $W_p = 0.5 \mu\text{m}$

i) Avalanche breakdown

$$E_{crit} (10^{18} \text{ cm}^{-3}) = 1.3 \cdot 10^6 \frac{\text{V}}{\text{cm}} \quad (\text{past lecture notes})$$

analysis equivalent to a)

plug-in numbers:

$$X_n' = \sqrt[0.65]{1.293 \cdot 10^{-6}} \text{ cm} = \sqrt[0.65]{1.293 \cdot 10^{-2}} \mu\text{m} = 8.4 \text{ nm}$$

$$X_p' = \sqrt[0.65]{1.293 \cdot 10^{-5}} \text{ cm} = \sqrt[0.65]{1.293 \cdot 10^{-1}} \mu\text{m} = 84 \text{ nm}$$

$$\phi_i = \frac{kT}{q} \ln \left(\frac{N_a N_d}{n_i^2} \right) = 1.02 \text{ V}$$

$$\phi_i - V_a = \frac{1}{2} E_{crit} (X_n' + X_p') = 8.04 \text{ V}$$

$$-V_a = 7.02 \text{ V}$$

ii) Punch-through breakdown

$$\left. \begin{array}{l} X_n' \ll W_n \\ X_p' < W_p \end{array} \right\} \Rightarrow \text{no punch-through}$$

iii) Zener breakdown

$$E_{crit}^{zener} = 1.4 \cdot 10^6 \frac{\text{V}}{\text{cm}} \approx E_{crit}^{avalanche}$$

Note:

Zener breakdown occurs at a slightly higher critical field than avalanche.

Breakdown will occur via both mechanisms, with avalanche dominant

4

$$N_a = 10^{19} \text{ cm}^{-3} \quad N_d = 10^{17} \text{ cm}^{-3} \quad \tau_n = \tau_p = 0.5 \mu\text{s}$$

$$W_p = 0.1 \mu\text{m} \quad W_n = 500 \mu\text{m} \quad V_a = 0.6 \text{ V (FW biased)}$$

$$V_{bi} = \frac{KT}{q} \ln \left(\frac{N_a N_d}{n_i^2} \right) = 0.93146 \text{ V}$$

$$x_n = \sqrt{\frac{2\epsilon V_{bi}}{q} \left(\frac{N_a}{N_d} \right) \left(\frac{1}{N_a + N_d} \right)} = 1.0918 \times 10^{-5} \text{ cm}$$

$$x_p = \sqrt{\frac{2\epsilon V_{bi}}{q} \left(\frac{N_d}{N_a} \right) \left(\frac{1}{N_a + N_d} \right)} = 1.0918 \times 10^{-7} \text{ cm}$$

$$D_n = \frac{KT}{q} \mu_n = 34.9$$

$$D_p = \frac{KT}{q} \mu_p = 12.41$$

$$L_n = \sqrt{D_n \tau_n} = 4.1773 \times 10^{-3} \text{ cm}$$

$$L_p = \sqrt{D_p \tau_p} = 2.49 \times 10^{-3} \text{ cm}$$

$$n_{p0} = n_i^2 / N_a = 22.5 \text{ cm}^{-3}$$

$$p_{n0} = n_i^2 / N_d = 2.25 \times 10^3 \text{ cm}^{-3}$$

$$W_p < L_n \Rightarrow \text{Short diode}$$

$$p_n(x_n) = p_{n0} \exp(2V_a / KT) = 2.70195 \times 10^{13} \text{ cm}^{-3}$$

$$n_p(x_p) = n_{p0} \exp(2V_a / KT) = 2.70195 \times 10^{14} \text{ cm}^{-3}$$

$$J_n(x) = q \frac{D_n n_{p0}}{W_p} \left[\exp\left(\frac{2V_a}{KT}\right) - 1 \right] = \text{~~2.1575 \times 10^{-2} A/cm^2~~}$$

$$J_n(W_p) = 0.15108 \text{ A/cm}^2$$

$$a) J_p(x_n) = q \frac{D_p p_{n0}}{L_p} \left[\exp\left(\frac{2V_a}{KT}\right) - 1 \right] = \boxed{2.1575 \times 10^{-2} \text{ A/cm}^2}$$

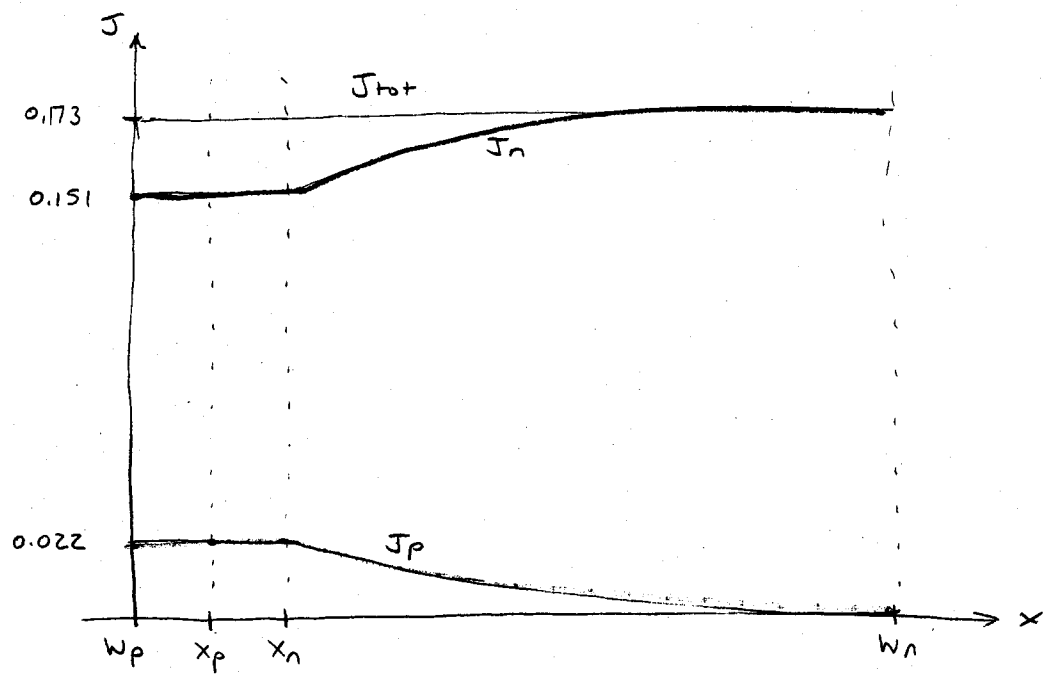
$$J_{\text{tot}} = J_p(x_n) + J_n(x_p) = 0.17265 \text{ A/cm}^2$$

$$b) J_p(x_p) = J_p(x_n) = \boxed{2.157 \times 10^{-2} \text{ A/cm}^2} \quad (\text{no recombination})$$

4

$$c) J_n(w_p) = q \frac{D_n n_{p0}}{w_p} [\exp(qV_a/KT) - 1] = 0.15108 \text{ A/cm}^2$$

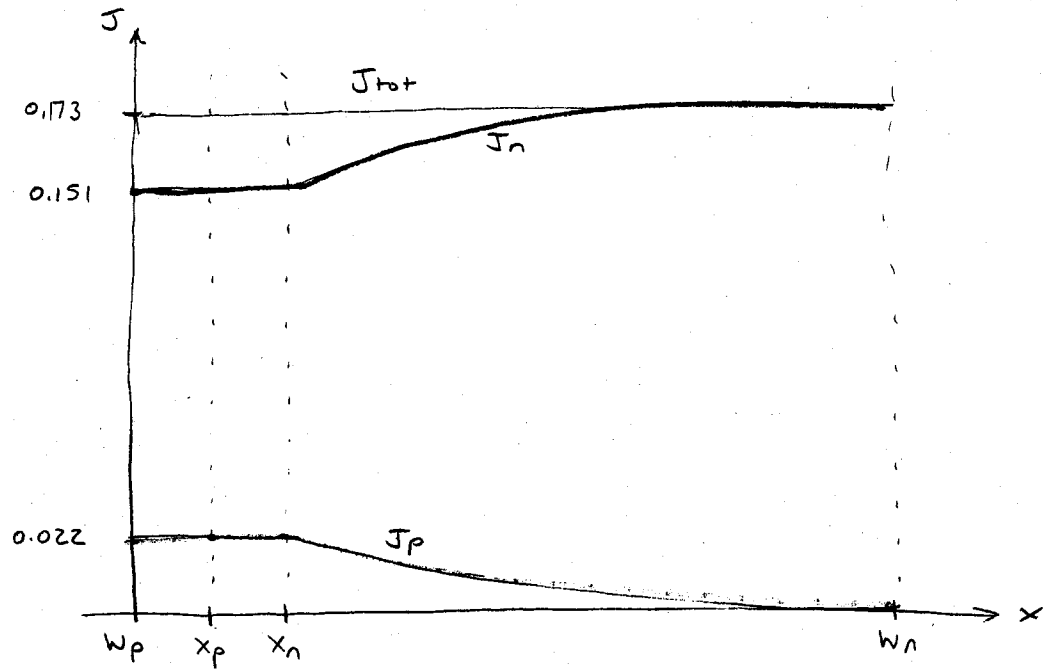
$$d) J_n(w_n) \approx J_{tot} = J_p(x_n) + J_n(w_p) = 0.17206 \text{ A/cm}^2$$



4

c) $J_n(w_p) = q \frac{D_n n_{p0}}{w_p} [\exp(qV_a/KT) - 1] = 0.15108 \text{ A/cm}^2$

d) $J_n(w_n) \approx J_{tot} = J_p(x_n) + J_n(w_p) = 0.17206 \text{ A/cm}^2$



$$p = \frac{10^{19}}{2} + \sqrt{\left(\frac{10^{19}}{2}\right)^2 + (1.5 \times 10^{10})^2} = 10^{19}$$

$$n = \frac{10^{19}}{n_{i2}} = 0.044 \text{ cm}^{-3} = n_{p0}$$

$$N_A = 10^{19} \quad N_D = 10^{17} \rightarrow n = 10^{17}, \quad p = \frac{10^{17}}{n_{i2}} = 4.94 \times 10^{-6} \text{ cm}^{-3} = p_{n0}$$

3a)

$$x_n = \left[\frac{2k\epsilon_0}{q} \phi_i \left(\frac{N_A}{N_D(N_A + N_D)} \right) \right]^{\frac{1}{2}} = \left[\frac{2(11.7)(8.85 \times 10^{-14})}{(1.6 \times 10^{-19})} (0.937) \left(\frac{10^{19}}{10^{17}(10^{19} + 10^{17})} \right) \right]^{\frac{1}{2}}$$

$$= 1.096 \times 10^{-5} \text{ cm}$$

$$x_p = \left[\frac{2k\epsilon_0}{q} \phi_i \left(\frac{N_D}{N_A(N_A + N_D)} \right) \right]^{\frac{1}{2}} = 1.096 \times 10^{-7} \text{ cm} = 1.096 \times 10^{-3} \mu$$

$$x_d = x_n + x_p = 1.107 \times 10^{-5} \text{ cm}$$

$$\Delta p = p_{n0} \left(\exp \frac{qV_a}{kT} - 1 \right) \exp -\frac{x - x_n}{L_p}$$

@ $x = x_n$ $\Delta p = (4.94 \times 10^{-6}) \left(\exp \frac{0.6}{0.026} - 1 \right) \exp -\frac{x_n - x_n}{L_p} = 4.673 \times 10^6 \text{ cm}^{-3}$

GENERAL: $\Delta p = 4.673 \times 10^6 \exp \left(-\frac{x - x_n}{0.00180} \right) \quad x > x_n$

@ $x = x_p$ $\Delta n = (0.044) \left(\exp \frac{0.6}{0.026} - 1 \right) \exp \frac{x + x_p}{L_n} = 4.631 \times 10^8 \text{ cm}^{-3}$

GENERAL: $\Delta n = 4.631 \times 10^8 \exp \left(\frac{x + x_p}{0.00127} \right) \quad x < x_p$

b) $I_p = qA \frac{p_{p0}}{L_p} \left(\exp \frac{qV_a}{kT} - 1 \right) \exp -\frac{x - x_n}{L_p} = \frac{(1.6 \times 10^{-19})(1.3)(4.94 \times 10^{-6})(A)}{0.00180} \left(\exp \frac{0.6}{0.026} - 1 \right) \exp -\frac{x - x_n}{L_p}$

$$I_p = 5.4 \times 10^{-10} (A) \exp -\frac{x - x_n}{0.00180}$$

$$I_n = qA \frac{n_{p0}}{L_n} \left(\exp \frac{qV_a}{kT} - 1 \right) \exp \frac{x + x_p}{L_n} = \frac{(1.6 \times 10^{-19})(20.8)(0.044)(A)}{0.00127} \left(\exp \frac{0.6}{0.026} - 1 \right) \exp \frac{x + x_p}{L_n}$$

$$I_n = 1.213 \times 10^{-6} (A) \exp \frac{x + x_p}{0.00127}$$

$$J_n = \frac{I_n}{A}$$

5 a)

$$p_n(x) = p_{n0} + p_{n0} e^{x/L_D} \left(e^{\frac{qV_a}{kT}} - 1 \right) e^{-x/L_D}$$

$$p_{n0} = \frac{n_i^2}{N_D}$$

$$n_p(x) = Ax + B \quad \text{where} \quad \begin{cases} A = \frac{n_{p0} \left(e^{\frac{qV_a}{kT}} - 1 \right)}{W_p - x_p} \\ B = n_{p0} + A W_p \end{cases}$$

$$n_{p0} = \frac{n_i^2}{N_A}$$

b) General form for Current Density:

$$J_{p_n}(x) = -q D_p p_{n0} e^{x/L_D} \left(e^{\frac{qV_a}{kT}} - 1 \right) \left(-\frac{1}{L_D} \right) e^{-x/L_D}$$

$$J_{np}(x) = q D_n \frac{n_i^2}{N_A} \frac{e^{\frac{qV_a}{kT}} - 1}{W_p - x_p}$$

5 c) Calculate the drift and diffusion components of the majority currents.

$$J_{\text{drift}}^n = -q \mu_n n(x) E(x)$$

$$J_{\text{drift}}^p = q \mu_p p(x) E(x)$$

$$J_{\text{diff}}^n = (-q) \underbrace{\left(D_n \frac{dn}{dx} \right)}_{\text{flux}}$$

$$J_{\text{diff}}^p = q \underbrace{\left(-D_p \frac{dp}{dx} \right)}_{\text{flux}}$$

$$J_{\text{diff}}^n = q D_n \frac{dn}{dx}$$

n-region: constant quasi-neutrality $\Delta n_n = \Delta p_n$

$$n_n(x) = n_{n0} + \Delta n_n(x) = n_{n0} + \Delta p_n(x)$$

$$i) \Rightarrow J_{\text{diff}}^{nn}(x) = q \cdot D_n \cdot \frac{dn_n}{dx} = q \cdot D_n \frac{d\Delta p_n}{dx}$$

from 4) $\Delta p_n(x) = p_n(x) - p_{n0} = p_{n0} e^{x/L_p} \left(e^{\frac{qV_g}{kT}} - 1 \right) e^{-x/L_p}$

$$\Rightarrow J_{\text{diff}}^{nn}(x) = q \cdot D_n \cdot p_{n0} e^{x/L_p} \left(e^{\frac{qV_g}{kT}} - 1 \right) \cdot \left(-\frac{1}{L_p} \right) \cdot e^{-x/L_p}$$

$$ii) \Rightarrow J_{\text{drift}}^{nn} = -q \mu_n n_n(x) E(x) = -q \mu_n n_{n0} E(x)$$

$n_n(x) \approx n_{n0}$ (low level injection)

p-region: quasi-neutrality $\Delta p_p = \Delta n_p$

$$p_p(x) = p_{p0} + \Delta p_p(x) = p_{p0} + \Delta n_p(x)$$

$\uparrow$ constant

$$i) \Rightarrow J_{\text{diff}}^{pp}(x) = -q D_p \frac{dp_p}{dx} = -q D_p \frac{d\Delta n_p(x)}{dx}$$

from 4) $\Delta n_p(x) = n_p(x) - n_{p0} = A \cdot x + B - n_{p0} =$

$$J_{\text{diff}}^{pp}(x) = -q D_p \cdot A = -\frac{q D_p \cdot n_{p0} \left(e^{\frac{qV_g}{kT}} - 1 \right)}{W_p - x_p}$$

$$A = \frac{n_{p0} \left(e^{\frac{qV_g}{kT}} - 1 \right)}{W_p - x_p}$$

$$B = n_{p0} + A W_p$$

5 c)

$$ii) J_{drift}^{pp} = q \mu_p p_p(x) E(x)$$

$$J_{drift}^{pp} = q \mu_p p_p E(x)$$

$p_p(x) \approx p_p$ (low level injection)

$$(1) J_{total} = J_{diff}^{pn} + J_{diff}^{nn} + J_{drift}^{nn}$$

$$(2) J_{total} = J_{diff}^{pn} + J_{drift}^{np} (-x_p) = \text{const.}$$

$$(1) = (2) \Rightarrow J_{drift}^{nn} = J_{total} - J_{diff}^{pn} - J_{diff}^{nn}$$

5 d) calculate $E(x)$ in n and p region outside the depletion region

n-region:

$$J_{drift}^{nn} = -q \mu_n n_{n0} E(x)$$

$$-q \mu_n n_{n0} E(x) = J_{total} - \frac{q D_p p_{n0}}{L_p} e^{x/L_p} (e^{qV_{bi}/kT} - 1) e^{-x/L_p} + \frac{q D_n n_{p0}}{L_p} (e^{qV_{bi}/kT} - 1) e^{-x/L_p}$$

$$E(x) = -\frac{1}{q \mu_n n_{n0}} \left(J_{total} + \frac{q p_{n0}}{L_p} e^{x/L_p} (e^{qV_{bi}/kT} - 1) (D_n - D_p) e^{-x/L_p} \right)$$

p-region:

$$J_{drift}^{pp} = q \mu_p p_p E(x)$$

$$(1) J_{total} = \text{const (see above)}$$

$$(2) J_{total} = J_{diff}^{np} + J_{diff}^{pp} + J_{drift}^{pp}$$

$$\Rightarrow J_{drift}^{pp} = J_{total} - J_{diff}^{np} - J_{diff}^{pp}$$

$$q \mu_p p_{p0} E(x) = J_{total} - \frac{q D_n n_{p0} (e^{qV_{bi}/kT} - 1)}{L_p - x_p} + \frac{q D_p p_{n0} (e^{qV_{bi}/kT} - 1)}{L_p - x_p}$$

$$\Rightarrow E(x) = \text{const}$$

5 e) Diff. approximation

minority J_{diff} neglectable

check

n-region:

$$J_{diff}^{pn} \ll J_{diff}^{pn}$$

$$J_{diff}^{pn} = q \mu_p p_n(x) E(x)$$

$$E(x) = \frac{1}{q \mu_n n_{n0}} (\dots)$$

$$\Rightarrow J_{diff}^{pn} \propto \frac{p_n(x)}{n_{n0}}$$

quasi-neutrality very small

$$\frac{p_n(x)}{n_{n0}} \approx \frac{\Delta p_n}{n_{n0}}$$

✓ low-level injection assumption

p-region:

$$J_{diff}^{np} = +q \mu_n n_p(x) E(x)$$

$$E(x) = \frac{1}{q \mu_p p_{p0}} (\dots)$$

$$\Rightarrow J_{diff}^{np} \propto \frac{n_p(x)}{p_{p0}} \approx \frac{\Delta p_p}{p_{p0}}$$

very small

(low level injection assumption)

→ if low level injection is ok diff. approx. is ok.

5 f) use currents to get charge densities as a function of position

idea: $\vec{\nabla} \cdot \vec{E} = \frac{\rho}{\epsilon_0}$

1-D $\frac{dE}{dx} = \frac{\rho(x)}{\epsilon_0}$

n-region:

$$E(x) = -\frac{1}{q\mu_n n_{no}} \left(J_{total} + \frac{q p_{no}}{L_p} e^{x/L_p} \left(e^{\frac{qV_0}{kT}} - 1 \right) (D_n - D_p) e^{-x/L_p} \right)$$

$$\frac{dE}{dx} = -\frac{1}{q\mu_n n_{no}} \cdot \frac{q p_{no}}{L_p} e^{x/L_p} \left(e^{\frac{qV_0}{kT}} - 1 \right) (D_n - D_p) \cdot \left(-\frac{1}{L_p} \right) e^{-x/L_p}$$

$$= \frac{p_{no}}{n_{no} L_p^2 / \mu_n} \left(e^{\frac{qV_0}{kT}} - 1 \right) (D_n - D_p) e^{-x/L_p} \stackrel{!}{=} \frac{\rho(x)}{\epsilon_0}$$

$$p_{no} = \frac{n_i^2}{N_d}$$

$$n_{no} = N_d$$

$$\Rightarrow \rho(x) = \epsilon_0 \left(\frac{n_i}{N_d} \right)^2 \cdot \frac{e^{x/L_p}}{L_p^2 / \mu_n} \left(e^{\frac{qV_0}{kT}} - 1 \right) (D_n - D_p) e^{-x/L_p}$$

p-region:

$$E(x) = \text{const}$$

$$\Rightarrow \frac{dE}{dx} = 0 \Rightarrow \rho(x) = 0$$

Quasi-neutrality assumption: $|p_{no}| \ll |q(N_a - N_d)|$

in p-region: completely fulfilled $\rho(x) = 0$

in n-region: $\rho(x) \propto \left(\frac{n_i}{N_d} \right)^2$

base: $n_i \ll N_d \Rightarrow \left(\frac{n_i}{N_d} \right)^2$ very small

$\rightarrow$ fulfilled up to a term $\propto \left(\frac{n_i}{N_d} \right)^2$