

1. (a) From the figure we have  $R_p = 50 \text{ nm}$ ,  $\Delta R_p = 18 \text{ nm}$  for both Si and  $\text{Si}_3\text{N}_4$ .

Since the thickness of  $\text{Si}_3\text{N}_4$  layer is 10 nm, the implanted peak is  $50 \text{ nm} - 10 \text{ nm} = 40$  nm away from the Si/ $\text{Si}_3\text{N}_4$  interface.

The implanted profile can be expressed as

$$C(x) = C_p \exp\left(-\frac{(x-R_p)^2}{2\Delta R_p^2}\right) = \frac{Q}{\sqrt{2\pi} \Delta R_p} \exp\left(-\frac{(x-R_p)^2}{2\Delta R_p^2}\right)$$

$$= 4.43 \times 10^{19} \text{ cm}^{-3} \exp\left(-\frac{(x-50 \text{ nm})^2}{2 \times (18 \text{ nm})^2}\right)$$

The implanted dose in Si is:

$$\int_{10 \text{ nm}}^{\infty} C(x) dx = \frac{Q}{2} \operatorname{erfc}\left(\frac{x_{\text{SiN}} - R_p}{\sqrt{2} \Delta R_p}\right)$$

$$= \frac{Q}{2} \operatorname{erfc}(-1.57) = \frac{Q}{2} \times 1.97$$

$$= 1.97 \times 10^{14} \text{ cm}^{-2}$$

(b)

The effective  $D_t$  for in TED is

$$(D_t)_{\text{TED}} = D_B \left[ \frac{Q R_p}{d_i C_i^*} \right] f_I \times 1.5 , \quad f_I = 1 \text{ for boron.}$$

The effective time for boron under equilibrium conditions should be

$$\frac{(D_t)_{\text{TED}}}{D_B} = 1.5 \times \left[ \frac{Q R_p}{d_i C_i^*} \right] = \frac{1.97 \times 10^{14} \text{ cm}^{-2} \times 50 \times 10^7 \text{ cm} \times 1.5}{5 \times 10^{25} \exp\left(\frac{-4.88}{8.62 \times 10^{-5} \times 1273.15}\right)} \cancel{\times 1}$$

$$= \frac{1.97 \times 50 \times 10^7 \text{ cm}^{-1} \times 1.5}{2.44 \times 10^6 \text{ cm}^{-1} \text{ s}^{-1}} = \cancel{604.5 \text{ s}}$$

The alternative method is by using  $t_{\text{eff}} = T_{\text{end}} \frac{C_2^{\text{max}}}{C_2^*} \times 1.5$

Here  $T_{\text{end}}$  is the duration of TED which is about 0.5 s in the plot;  $C_2^{\text{max}}/C_2^*$  is the supersaturation of interstitial which is about 800 in the plot;

$\angle 111$  wafer

2.

In steam at  $100^\circ\text{C}$  we have

$$B = 3.86 \times 10^8 \text{ nm}^2 \text{ hr}^{-1} \exp\left(-\frac{0.78}{8.62 \times 10^{-5} \times 1273.15}\right)$$

$$= 0.3162 \text{ nm}^2/\text{hr}$$

$$\frac{B}{A} = 1.63 \times 10^8 \text{ nm/hr} \exp\left(\frac{-2.05}{8.62 \times 10^{-5} \times 1273.15}\right)$$

$$= 1.2582 \text{ nm/h}$$

$$\Rightarrow A = 0.2513 \text{ nm}$$

$$t = \frac{x_i^2}{B} + \frac{x_i}{B/A} = \frac{(0.2 \text{ nm})^2}{0.3162 \text{ nm}^2/\text{hr}} + \frac{0.2 \text{ nm}}{1.2582 \text{ nm/h}} = 0.2855 \text{ hr}$$

\* The final oxide thickness is

$$x_0 = \frac{A}{2} \left[ \sqrt{1 + \frac{t + t_c}{A^2/4B}} - 1 \right] = 0.1256 \text{ nm} \left[ \sqrt{1 + \frac{(2 + 0.2855) \text{ hr}}{0.2513/(4 \times 0.3162)}} - 1 \right]$$

$$= 0.1256 \text{ nm} [\sqrt{1 + 45.77} - 1] = 0.733 \text{ nm}$$

3. If an initial 200nm oxide on a <100> wafer is further oxidized in pure O<sub>2</sub> at 1000°C, what would be the interstitial supersaturation near the beginning of the growth process and the resulting diffusion enhancement factor (D/D\*) for As? (20)

$$\left. \begin{aligned} \frac{dx_0}{dt} &= \frac{B}{2x_0 + A} \\ &= \frac{0.0105 \mu\text{m}^2/\text{hr}}{2(0.2 \mu\text{m}) + 0.233 \mu\text{m}} \\ &= 0.0166 \frac{\mu\text{m}}{\text{hr}} \end{aligned} \right\} \left. \begin{aligned} B_{100} &= B_{III} = 7.72 \times 10^2 \exp\left(-\frac{1.23 \text{ eV}}{kT}\right) \frac{\mu\text{m}^2}{\text{hr}} \\ &= 0.0105 \mu\text{m}^2/\text{hr} \end{aligned} \right\}$$

$$\left. \begin{aligned} \frac{B}{A_{100}} &= \frac{B}{A_{III}} / 1.68 = \frac{6.23 \times 10^6}{1.68} \exp\left(-\frac{2.0 \text{ eV}}{kT}\right) \frac{\mu\text{m}}{\text{hr}} \\ &= 0.045 \mu\text{m}/\text{hr} \end{aligned} \right\}$$

$$A_{100} = \frac{B}{B/A} = \frac{0.0105 \mu\text{m}^2/\text{hr}}{0.045 \mu\text{m}/\text{hr}} = 0.2333 \mu\text{m}$$

From  $\frac{\langle D_p \rangle}{D_p^*}$  vs  $\left\langle \frac{dx_0}{dt} \right\rangle$  plot

$$\frac{\langle D_p \rangle}{D_p^*} \approx 4 = f_I^P \frac{C_I}{C_I^*} + f_V^P \frac{C_V}{C_V^*}$$

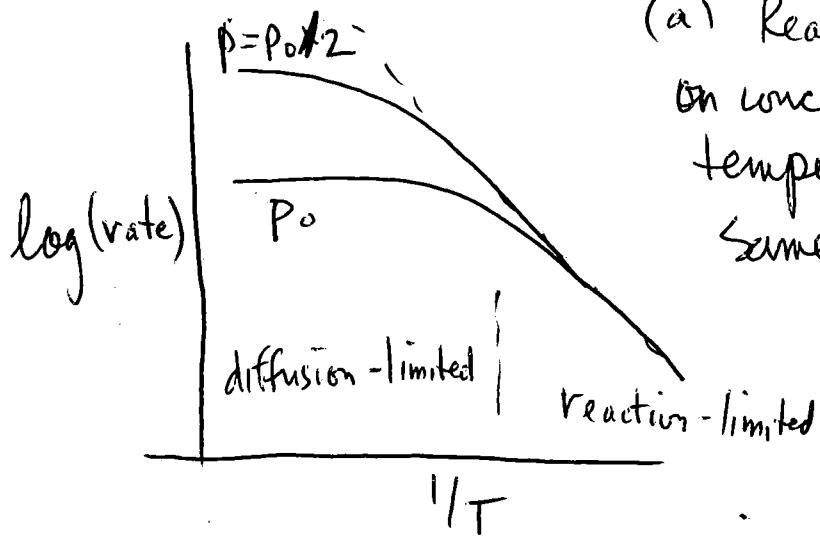
Assuming  $\frac{C_V}{C_V^*} = \frac{C_I^*}{C_I}$   
and using  $f_I = 0.98$

$$\frac{C_I}{C_I^*} = 4.08$$

$$\frac{\langle D_{As} \rangle}{D_{As}^*} = f_I^{As} \left( \frac{C_I}{C_I^*} \right) + f_V^{As} \left( \frac{C_V}{C_V^*} \right) = 0.4(4.08) + \frac{0.6}{4.08}$$

$$= \underline{\underline{1.76}}$$

4. Sketch the deposition rate versus temperature for an LPCVD polysilicon deposition process with SiH<sub>2</sub>Cl<sub>2</sub>/H<sub>2</sub> source gasses. If the pressure is dropped by a factor of 2, but the SiH<sub>2</sub>Cl<sub>2</sub> partial pressure is kept the same, what will happen to the deposition rate (increase, decrease, no change) if the process is (a) reaction limited and (b) diffusion limited. Briefly explain answer in each case. (18)

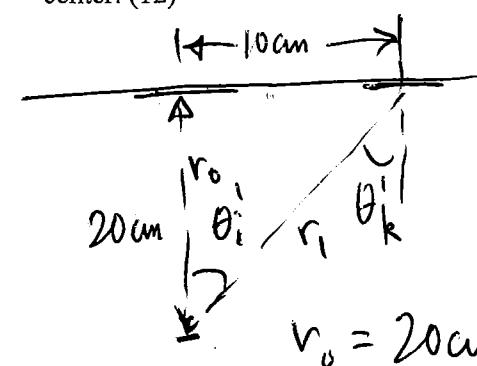


(a) Reaction limited process depends only on concentration of reactant(s) and temperature. These both remain the same, so no change.

(b) Mass transport in gas phase depends on total pressure inversely ( $D \propto 1/P_{\text{total}}$ ) and  $h$  (gas phase mass transfer rate) is proportional to  $D$ .

Thus if pressure is dropped, growth rate will increase. Increase will be a factor of 2 if thickness of stagnant layer (which varies much less strongly with pressure) is unchanged.

5. In an evaporation chamber, wafers are attached to a flat wafer holder parallel to and 20 cm away from the small area source. If the angular distribution of the source is ideal ( $n=1$ ), what would be the ratio of deposition rates on a flat wafer surface between the center of the wafer holder (directly opposite source) and 10 cm away from the center. (12)



$$\text{rate} \propto \frac{1}{r^2} \cos^n \theta_i \cos \theta_k \quad n=1$$

$$\frac{\text{rate}(x=0)}{\text{rate}(x=10\text{cm})} = \frac{1/r_o^2 \cos(0) \cos(0)}{1/r_i^2 \cos(\theta_i) \cos(\theta_k)}$$

$$r_o = 20\text{cm}$$

$$r_i = \sqrt{(20\text{cm})^2 + (10\text{cm})^2}$$

$$\text{Ans } \theta_i = \theta_k, \cos \theta_k = \frac{20\text{cm}}{\sqrt{(20\text{cm})^2 + (10\text{cm})^2}}$$

$$\frac{\text{rate}(x=0)}{\text{rate}(x=10)} = \frac{\frac{1}{(20\text{cm})^2} (1) (1)}{\frac{1}{(500\text{cm}^2)} \frac{400\text{cm}^2}{500\text{cm}^2}} = \left(\frac{5}{4}\right)^2 = \frac{25}{16} = 1.5625$$